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| DEPARTMENT OF TRANSPORTATION <br> BUREAU OF BRIDGES AND STRUCTURES | CULVERT MANUAL CHANGE LETTER NO. 17-01 |
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This Culvert Manual revision includes several minor and editorial changes throughout the manual and three major changes as well. The following is a brief summary of the three major changes:

## Section 4 - "Headwalls and Wingwalls"

- Revised Fig. 4.1.5-1, headwall reinforcement slightly increased
- Revised Table 4.2.2-1, reinforcement size revised to require smaller bars at tighter spacing instead of larger bars at larger spacing
- Revised T-Type Design Tables

The following is a summary of the minor revisions:

- Section 2.1.3.1, revised description of when Hydraulic Reports and Structure Geotechnical Reports are required
- Sections 2.2.1.2, 2.2.2.3, revised pay item "Membrane Waterproofing for Culverts" to "Membrane Waterproofing for Buried Structures"
- Sections 2.5.2, 2.5.3, removed 3'-6" minimum dimension for distance from Stage Removal Line to inside of Temporary Concrete Barrier
- Section 3.5.12, fixed typographical error in shear capacity equation
- Sections 4.1.1.1, 4.1.1.2, revised description of design assumptions for loading
- Figure 4.1.3.1-1, revised typographical error
- Section 4.1.5, added references to headwall drain and concrete collar details
- Figure 4.2.2-3, added $y$-axis label to figure
- Section 4.3.1, revised height of counterfort
- Section 4.4.3, revised T-Type wingwall example to match new tables

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# Culvert Manual 

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## Section 1 Introduction

As directed by the Engineer of Bridges and Structures, it is the responsibility of the Engineer of Bridge Design to develop, maintain, and administer the policies that govern the design and preparation of plans and specifications for all structures under the jurisdiction of the Department of Transportation. The vehicle by which this policy is controlled is the Bridge Manual.

This manual is a supplement to the Bridge Manual. The purpose of this manual is to aid in the design and detailing of reinforced concrete box culverts. Presented herein is a compilation of design procedures, design charts and tables, and standard tables. Base sheets, available at http://www.idot.illinois.gov/doing-business/procurements/engineering-architectural-professional-services/Consultants-Resources/bridges-and-structures-cadd-downloads-and-guidelines are referenced herein as well.

This manual is an active manual in the respect that as research, revised criteria, and AASHTO specification revisions dictate, new or revised sheets will be issued. It is strongly urged that as these sheets are received, they be immediately incorporated in the book so that the manual's integrity is maintained.

## Section 2 Planning

This section of the Culvert Manual provides guidance for the majority of box culverts in Illinois, which are either precast concrete box culverts or cast-in-place concrete box culverts. Other culvert types, such as metal culverts and pipe culverts, will not be discussed in this manual.

The Bureau of Bridges and Structures is available to assist the Districts and local public agencies in resolving any problems that may arise during plan development and clarifying any questions relative to the interpretation of these requirements.

### 2.1 General Planning Process

### 2.1.1 Culvert Determination

The determination of whether a structure over a waterway should be a culvert, a three sided precast concrete structure, or a bridge is heavily influenced by hydraulic opening requirements. As the hydraulic opening becomes larger, the selection process for structure type progresses from culvert to three sided precast concrete structure to bridge. Cost, future maintenance, profile grade, staging, skew, soil conditions and alignment are also important variables which should be considered. Culverts generally have low future maintenance; however, culverts should not be considered for waterways with a history or potential of debris accumulation.

### 2.1.2 Culvert Type Selection

In general, precast concrete box culverts are more economical than cast-in-place concrete box culverts. One advantage of precast culverts is the economy that results from the duplication of forms, elimination of most falsework, and the need for only a small construction crew. Precast construction is particularly convenient in places where labor and material are not readily available. Use of precast units allows rapid repair or replacement of existing structures without detours and with minimum interference to traffic. However, complications such as poor soils, stage construction issues, and limited contractor access to the site may warrant the use of cast-in-place concrete box culverts. Discretion is given to the District or Owner on the use of precast concrete box culverts. Precast culverts are also an acceptable option for pedestrian tunnels.

### 2.1.3 Culvert Processing Requirements

### 2.1.3.1 Single Barrel Concrete Box Culverts

Existing culverts with a clear span greater than or equal to 6 ft . require a Bridge Condition Report (BCR). For state structures, new culverts with clear spans greater than or equal to 6 ft . require a structure number. New culverts do not require a Type Size and Location plan (TSL plan) if the design can be performed using the standard design tables found within this manual. Hydraulic Reports and Structure Geotechnical Reports and/or subsurface investigations may be required. See Section 6-106 of the Drainage Manual and Section 7.4 of the Geotechnical Manual for more information. The responsibility of development of design plans remains with the Districts, with assistance from the BBS as needed. BBS will provide assistance on design of new culverts not meeting Design Table requirements and in need of special design.

See the Bureau of Local Roads and Streets Manual for guidance on Local Agency culverts.

### 2.1.3.2 Multi-Barrel Cast-in-Place Concrete Box Culverts

For State structures, all new multi-barrel cast-in-place box culverts require a structure number. The plan preparation and structural design of this type of culvert remains with qualified consultants or the BBS in conformance with current plan development procedures. Items required to initiate the development of final detailed plans for culverts may include:

1. Bridge Condition Report (BCR)
2. Hydraulic Report
3. Structure Geotechnical Report (SGR) and subsurface investigation
4. TSL Plan

Additional references for the above items may be found in Section 2.2 and Section 2.3 in the Bridge Manual, as well as in "Bridge Condition Report Procedures and Practices," an IDOT document.

See the Bureau of Local Roads and Streets Manual for guidance on Local Agency culverts.

### 2.1.3.3 Multi-Barrel Precast Concrete Box Culverts

Consistent with current processing procedures for all multi-barrel culvert projects, submittal of a BCR to the BBS for review and approval may be required for State structures.

For State structures, the option to use multi-barrel precast concrete box culverts is at the discretion of the Districts and should be decided prior to the TSL plan phase. If the location meets the foundation requirements and general guidelines and design limitations for a multibarrel precast concrete box culvert, the Districts can undertake the final plan development.

The processing of TSL plans or final plans for multi-barrel precast concrete box culverts to the BBS for review and approval will not be required except for structures on the interstate system. See the Bureau of Local Roads and Streets Manual for guidance on Local Agency culverts.

### 2.1.4 Culvert Use Limitations

Cambering the box will not be allowed for precast concrete box culverts.

A minimum cover of 6 in., measured from the bottom of the pavement surface to the top of the top slab, taken at the roadway edge, shall be provided for precast concrete box culverts. Cast-in-place concrete box culverts may be used in zero-fill situations.

All headwalls for multiple-cell precast concrete box culverts shall be collared around the end of the precast sections. Due to the size and weight of these units, it is anticipated that headwalls for multiple-cell precast concrete box culverts will be cast-in-place similar to the details shown on Base Sheets MCB-AES-1 and MCB-AES-2. Individual precast end sections similar to those detailed in Base Sheets MCB-TES-1 and MCB-TES-2 may be used if hydraulically acceptable.

Precast concrete box culvert designs shall provide hydraulic equivalence to conventional cast-in-place designs. This may occasionally require a larger precast culvert size to compensate for the additional inlet losses and the adjustment to standard sizes.

The use of multiple cell precast concrete box culverts is not recommended under the following conditions:
a. Where high settlement could be anticipated.
b. Where design flood velocity and stream bed soils raise concern for scour.
c. Where clogging from debris or sedimentation is a concern.

The Bureau of Bridges and Structures shall be consulted before use of precast concrete box culverts in locations where high seismic activity may occur.

The BBS is available to assist the District and local agencies in working out any problems that may arise during final plan development and clarifications of any questions relative to the interpretation of these requirements.

### 2.2 Concrete Box Culvert Types

### 2.2.1 Cast-in-Place Concrete Box Culverts

### 2.2.1.1 Single-Barrel Cast-in-Place Concrete Box Culvert Design Tables

Standard designs for single-barrel cast-in-place concrete box culverts for a range of sizes from 3 ft . x 2 ft . to 12 ft . x 12 ft . are given in Section 3.6. For new cast-in-place concrete box culverts, the clear span and clear height should be dimensioned in 1 ft . increments. For extensions of existing culverts, cast-in-place concrete box culverts should be dimensioned and detailed according to current policy.

Designers should be aware that Article 540.08 of the Standard Specifications provides an option to the contractor to substitute a precast box when a cast-in-place box has been shown in the plans. If a precast box substitution is not desirable, the following note shall be added to the TSL and final Contract Plans:

Precast option is not allowed.

### 2.2.1.2 Cast-in-Place Concrete Box Culvert Waterproofing and Sidewall Drainage

All cast-in-place box culverts with 3 ft . or less of fill shall be waterproofed using Membrane Waterproofing for Buried Structures. When required, the Membrane Waterproofing for Buried Structures shall extend down the sidewall a minimum of 1 ft . below the joint between the top slab and sidewall. Weep holes shall be provided in the sidewalls.

For pedestrian tunnels, sidewall drainage shall be accomplished by using geocomposite wall drains and pipe underdrains for structures. Weep holes shall be omitted for these structures. See Figure 2.2.1.2-1 for details.


Figure 2.2.1.2-1

### 2.2.1.3 Phoebe Nesting Site Details

Multi-barrel cast-in-place culverts with a clear height of 4 ft . -0 in . and greater shall be provided with phoebe nesting site details. These details consist of 1 in . ledges, 4 ft . -0 in . long, on each side of all interior walls near the downstream end when these walls contain a single plane of reinforcement bars located at the wall center. These ledges provide suitable nesting sites for certain bird species (phoebes and barn swallows) that tend to nest in man-made shelters. The ledge detail is depicted in Figure 2.2.1.3-1.


Figure 2.2.1.3-1

### 2.2.2 Precast Concrete Box Culverts

One advantage of precast culverts is the economy that results from the duplication of forms, elimination of most falsework, and the need for only a small construction crew. Precast construction is particularly convenient in places where labor and material are not readily available. Use of precast units allows rapid repair or replacement of existing structures with minimum interference to traffic.

Precast culverts may be manufactured using conventional structural concrete and forms (formed) or dry cast with vibrating form pipe making methods (machine-made). Standard sizes and dimensions are shown in ASTM C1577 and standard sizes are listed in Table 2.2.2.1-1.

Installation, Method of Measurement and Basis of Payment for Precast Concrete Box Culverts are included in the Standard Specifications. The Standard Specifications also require joints between units to be sealed to assure no embankment material is allowed to pass through.

### 2.2.2.1 Standard Precast Concrete Box Culvert Sections

Precast concrete box culverts range in size from 3 ft . x 2 ft . to $12 \mathrm{ft} . \times 12 \mathrm{ft}$., where the first number is the clear span and the second number is the rise, or clear height. The designs and details for these culverts are dictated by ASTM C1577 and Bureau of Design and Environment Special Provision. The culvert designs found in ASTM C1577 meet the requirements of the AASHTO LRFD Bridge Design Specifications. Standard precast concrete box culvert sizes are found in Table 2.2.2.1-1.

| Standard Precast Concrete Box Culvert Configurations <br> (Span $\times$ Rise -ft .) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $3 \times 2$ | $6 \times 3$ | $8 \times 3$ | $9 \times 8$ | $11 \times 2$ | $12 \times 4$ |
| $3 \times 3$ | $6 \times 4$ | $8 \times 4$ | $9 \times 9$ | $11 \times 3$ | $12 \times 5$ |
|  | $6 \times 5$ | $8 \times 5$ |  | $11 \times 4$ | $12 \times 6$ |
| $4 \times 2$ | $6 \times 6$ | $8 \times 6$ | $10 \times 2$ | $11 \times 5$ | $12 \times 7$ |
| $4 \times 3$ |  | $8 \times 7$ | $10 \times 3$ | $11 \times 6$ | $12 \times 8$ |
| $4 \times 4$ | $7 \times 2$ | $8 \times 8$ | $10 \times 4$ | $11 \times 7$ | $12 \times 9$ |
| $5 \times 2$ | $7 \times 4$ | $9 \times 2$ | $10 \times 6$ | $11 \times 9$ | $12 \times 11$ |
| $5 \times 3$ | $7 \times 5$ | $9 \times 3$ | $10 \times 7$ | $11 \times 10$ | $12 \times 12$ |
| $5 \times 4$ | $7 \times 6$ | $9 \times 4$ | $10 \times 8$ | $11 \times 11$ |  |
| $5 \times 5$ | $7 \times 7$ | $9 \times 5$ | $10 \times 9$ |  | $12 \times 10$ |
|  |  | $9 \times 6$ | $10 \times 10$ | $12 \times 2$ |  |
| $6 \times 2$ | $8 \times 2$ | $9 \times 7$ |  | $12 \times 3$ |  |
|  |  |  |  |  |  |

Table 2.2.2.1-1

Planners considering a precast culvert should use standard sizes. The use of non-standard size boxes should be limited to structures with geometric limitations, such as extensions of existing non-standard culverts. Precast concrete box shapes not found in Table 2.2.2.1-1 are a special design and the designer shall provide the structural design in the contract plans.

### 2.2.2.2 Precast Concrete Box Culvert Plan Details

Precast concrete box culverts with precast concrete end sections require very few details on plan sheets. The plan and profile sheets in the roadway plans should state the box station location, size, maximum and minimum design fill heights, upstream and downstream invert elevations, and the culvert skew with respect to the roadway. The Contractor requires these details to be able to order the correct box from the precast concrete fabricator and properly install the culvert. Additional standard end section details may be required depending upon the
end section chosen. See Base Sheets SCB-TES, SCB-AES, MCB-TES, and MCB-AES for details. Note that these base sheets are all two sheets in length.

See Article 3.4.1 of this manual for direction on calculation of fill height.

### 2.2.2.3 Precast Concrete Box Culvert Waterproofing and Sidewall Drainage

All precast concrete box culverts under 3 ft . of fill or less shall be waterproofed using Membrane Waterproofing for Buried Structures. Precast concrete box culverts with more than 3 ft . of fill may be waterproofed at the request of the District. When waterproofing is required it shall extend down the sidewall a minimum of 1 ft . from the top of the culvert.

When used in a pedestrian tunnel application, the joints between precast concrete box culvert segments shall be sealed and the barrel covered with Membrane Waterproofing for Buried Structures. To provide for drainage, Geocomposite Wall Drains and Pipe Underdrains for Structures shall be used in lieu of weep holes. See Figure 2.2.2.3-1.


Figure 2.2.2.3-1

### 2.3 Hydraulics

The invert elevations of all culverts at stream crossing locations shall be set a minimum of 3 in . below the lowest point in the stream cross section. The intent is that culvert inverts will not become a barrier to fish migration during low water. The size of the culvert opening does not need to be increased to compensate for lowering the invert 3 in. Locations which may warrant lower invert elevations shall override this policy.

Scour or erosion at a bridge pier can create the possibility of catastrophic failure; however, since that is typically not the case at culvert structures, the FHWA does not mandate a calculation or evaluation of scour for this structure type. Although not considered a scour evaluation, the potential for damaging erosion, channel migration and aggradation\degradation are still addressed within the TSL plan development. This assessment can lead to the inclusion of such design features as riprap placement at one or both ends, cutoff walls, drop structures, energy dissipaters or even a change in structure type.

### 2.4 Foundations

Many of the foundation type issues discussed under Foundation Component Selection in Section 2.3.6.3 of the Bridge Manual are also applicable to foundations for box culverts. The SGR should provide planning and design recommendations to determine the most cost effective and feasible foundation treatment to be used on the TSL plans.

Box culverts have the following unique geotechnical issues that should be evaluated to ensure adequate long term performance of both the box and the wingwalls.

### 2.4.1 Settlement

The most common issues affecting the box portion of a culvert structure are mitigating differential settlement and ensuring constructibility of the bottom slab. Boxes are often located in existing stream channels where the new loading from a culvert and fill above will likely generate some settlement. It should be noted that the theoretical new loading at the base of the box is not as large as the new full height of soil fill loading adjacent to the box which can result in differential settlement along the roadway alignment. Since portions of the new box alignment
are often located on previously unloaded channel sediments while other segments may be placed through preloaded existing embankment, concern for differential settlement along the box alignment should also be considered. Consequently, it is critical that the designer and SGR author evaluate the variation in applied loadings as well as the changes in foundation soil conditions to determine if any ground modification is necessary.

### 2.4.1.1 Cast-in-Place Concrete Box Culverts

Cast-in-place boxes have some tolerance to span across settlement prone areas, but can crack when the differential foundation support is excessive. As an alternative to ground modification, a box can be designed and constructed in non-continuous segments which are jointed by collars to allow articulation and prevent overstress. Known as segmenting and cambering, the collar joints are placed at locations where changes in surcharge loading or foundation stiffness occur, and constructed at an elevation which will settle into the desired location. The most common configuration involves dividing the box into three segments with the center segment located directly below the level portion of the embankment. The center segment and its collars are detailed to be constructed above the desired flow line by 90 to $110 \%$ of the amount of estimated settlement, while the remaining outer segments slope from the collar to the top of the cutoff wall, which is normally located above the flow line by about 10 to $25 \%$ of the estimated settlement amount.

### 2.4.1.2 Precast Concrete Box Culverts

The use of multiple cell precast concrete box culverts set directly on rock should be avoided.

Precast boxes are articulated and can handle some differential settlement. However, when excessive movement is expected, the joints between the box sections can separate, causing the geotextile joint fabric to fail and allow soil to enter the box. In some cases, joint separation may decrease, causing contact and damage to the precast units. For these reasons, precast box culverts are normally only used at sites where minor amounts of settlement are expected or at locations where the foundation soils have been modified to mitigate settlement.

### 2.4.2 Removal and Replacement of Unsuitable Material

Where inadequate soil conditions are present to support the proposed loadings of either precast or cast-in-place boxes, removal of these soils and replacement with a coarse aggregate (or in less severe cases, re-compacted cohesive embankment) can be an economical treatment which provides the required stiffness or uniformity in foundation support. The cost effectiveness of this solution versus other ground modifications or structure type changes should be verified.

Removal and replacement is normally used when removal depths are not excessive, since concerns over cut slope stability or feasibility of stage construction soil retention can necessitate the use of other options. Removal and replacement also typically requires some field verification and adjustment to plan limits in order to address local problem zones or areas of uncertainty between borings. The designer should determine and show in the plan view the horizontal limits (stations and offsets) of the removal at the base of the excavation. The elevation view should show the elevations at the base of the removal. The plan and elevation removal limits should closely correspond to the boring data so that the inspector can determine the material the designer intends to be removed and what can remain. Since conditions encountered when excavation can differ, the Geotechnical and Field Construction Engineers may need to extend or reduce the limits to address the as encountered conditions. Along with the plan and elevation limits, the following note should be included.

The limits and quantities of removal and replacement shown are based on the boring data and may be modified by the District Geotechnical and Field Engineers for variable subsurface conditions encountered in the field.

Excavation of unsuitable material shall be paid for as "Removal and Disposal of Unsuitable Material for Structures". The replacement material and capping requirements are dependent upon the application, considering the anticipated loading, placement conditions, structure settlement tolerance, and cost of the replacement material. In cases such as replacement below box culverts where dewatering and compaction may not be possible, the pay item "Rockfill" is commonly used. In these cases, the following note should be added.

The Rockfill shall be capped with 6 in. of CA7 and satisfy the Standard Specifications unless otherwise indicated in the Special Provisions. The cost of the capping material shall be included in the pay item for Rockfill.

In cases where the replacement material strength requirements are less than $Q_{u}=1.25$ tsf., the placement conditions are well above the water table and quantities are relatively large, embankment can be specified as the replacement material since it is less expensive. Figure 2.4.2-1 gives an example of elevation and plan view details for removal and replacement.


Figure 2.4.2-1

### 2.4.3 Working Platform

When no removal and replacement is required, the foundation soils can become unstable due to construction equipment loadings during excavation, rebar placement, forming and concrete placement. In these cases, the Contractor may need a working platform to properly construct the culvert bottom slab. The need for such platforms is dependent on the type, thickness and strength of the soils encountered, the method of water diversion selected by the Contractor, precipitation, construction sequence, and the time of the year the box is constructed.

Since the borings are often taken in locations that do not give the designer accurate information about the sediment in the channel and considering the many factors cited above that affect the need for a platform, the designer is usually not in a position to specify its use and thus should not specify working platforms in the plans. The Field Engineer or District Geotechnical Engineer should make the determination that a working platform is required during excavation based on the field conditions. Thus, any removal indicated on the plans is understood to be related to the long term foundation performance of the box and embankment, rather than a tool to facilitate construction. When the estimated water surface elevation of the stream water is 4 ft . or more above the streambed, construction of a water diversion system may be very difficult. Maintaining dry conditions for bottom slab construction can be problematic in granular foundation soils below the water table, as their permeability may not allow normal pumping to keep up with the water inflow through these soils.

### 2.4.4 Wingwalls

In addition to the geotechnical issues discussed above affecting the box portion of the culvert, the culvert wingwalls are the other important element that is heavily influenced by the foundation soils and wall backfill.

### 2.4.4.1 Horizontal Cantilever Wingwalls

In most cases, a horizontal cantilever wingwall is the most economical and preferred wall type. They are supported by the box rather than the foundation soils, and their feasibility evaluation is therefore structural rather than geotechnical.

### 2.4.4.2 L-Type Wingwalls

In cases where the culvert height and/or wing length/skew will not permit the use of horizontal cantilever wingwalls, L-type wingwalls may be used. The L-type wingwall is structurally connected to the box at the cutoff wall, via the wing footing/bottom slab connection, as well as vertically along the wall/culvert interface. The foundation soils, particularly those furthest from the box, assist in providing vertical and lateral support.

### 2.4.4.3 T-Type and Miscellaneous Type Wingwalls

When L-type wingwalls are inadequate, or if precast box culverts are used, other soil dependent/box-independent wingwalls should be used. These wingwalls include T-type, mechanically stabilized earth (MSE), gabion, sheet piling, soldier piling, apron supported, and precast modular. MSE walls are normally not economical due to the small quantity, and they raise concerns in some hydraulic applications about loss of granular backfill or foundation soils.

T-type wingwalls are fairly common as their aesthetics, alignment and foundation design can be modified to accommodate most any application. However, the resulting foundation expense, particularly when either a cofferdam or piles are required, may suggest that another wingwall type may be more appropriate.

Gabion wingwalls can be specified to follow a wide range of curved alignments and face batters. They can be placed through limited depths of water, but should be supported on reasonably good foundations soils to resist overturning and bearing pressures.

Sheet pile walls also allow installation through open water and at locations where bearing capacity may not be adequate for other wall types.

Soldier piles are used where sheeting cannot be driven, as H-piles can penetrate farther or can be drilled when required. However, they require either a cast-in-place or other facing system.

Standard designs for precast end sections for use with traversable pipe grates are given on Base Sheets SCB-TES and MCB-TES. These are preferred when adequate right-of-way is
provided. If adequate right-of-way is not provided, cast-in-place aprons are often used with precast boxes. Standard designs for cast-in-place apron end sections are given on Base Sheets SCB-AES and MCB-AES.

Various precast modular wingwall systems have also been used, most commonly with precast box culverts to make the entire structure precast.

### 2.5 Constructability

Issues such as contractor access, formwork removal, and stage construction can affect constructability of culverts.

### 2.5.1 Contractor Access

Precast concrete box culvert sections require equipment to lift them into place. For larger precast concrete box culvert sections, this equipment can become very large and issues may arise in areas of low clearances or narrow right-of-way. In these cases, use of a cast-in-place concrete box culvert may be required.

Use of cast-in-place concrete box culverts is strongly discouraged for culverts with less than four feet of rise or span. This is because the formwork required for the top slab is difficult to remove under such tight conditions. While tables are given in Chapter 3 for cast-in-place culverts as small as three feet by two feet, these tables are intended to be used when no other options are available.

### 2.5.2 Minimum Clearance Width Requirements at the Stage Removal Line

A temporary concrete barrier or temporary bridge rail is required at all stage removal lines.

A minimum of $1^{\prime}-0$ " between the stage removal line and Stage I Construction should be provided to allow room for the contractor to install and remove formwork at the stage line. It will also provide clearance for the contractor to remove the remainder of the existing structure during Stage II removal without damaging the new culvert.

If soil retention on either side of the existing structure is required, temporary sheet piling or a temporary soil retention system is typically used. Geotextile walls are another alternate. Temporary sheet piling requires a minimum of 1 ft .- 6 in . clearance width for installation, and a temporary soil retention system may require more space due to the possible necessity of wales. This extra space requirement may force the planner to move the stage construction line, possibly causing right-of-way concerns or adding temporary pavement to the contract.

For culverts with fill, the slope from the bottom of the existing pavement to the top of the existing structure should be assumed to be 1:1. See Figure 2.5.2-1.

If one foot or less of retained fill is required on top of culverts, a railroad tie or a similar nonstructural headwall can be added to help retain the soil at the removal line. See Figure 2.5.2-1. This is minimally effective; little additional width is gained and may cause problems with clearance for a soil retention system. The railroad tie provides no additional structural strength at an unstiffened edge.

For culverts with large fills, a temporary soil retention system on top of the existing culvert may be required. The soil retention system should be assumed to be a minimum of $1^{\prime}-6$ " wide. See Figure 2.5.2-1. For larger retained heights, assume a temporary retention system that requires a sheet and wale system will be required. This system may be significantly wider than $1^{\prime}-6$ ". Sheet pile and wale systems three feet in width are common, and even wider systems may be required if the retained height is very large. See Section 3.13.1 of the Bridge Manual for more details.


Figure 2.5.2-1

### 2.5.3 Temporary Support System Requirements at Stage Removal Line

The adequacy of the existing structure to carry traffic under stage conditions must be assessed. Consideration must be given to the strength and stability of the structure once it has been partially removed and also to the overall condition of the structure. A structure may be found to be theoretically adequate to carry the loads, but because of deterioration there may be little confidence that it can do so safely.

The Stage I removal line is generally parallel to the centerline of the roadway. For existing skewed box culverts with reinforcement perpendicular to the sidewalls, this will require cutting of the primary reinforcement in the top and bottom slabs. See Figure 2.5.3-1. For skewed structures where the primary reinforcement is cut at the stage line, the edge of the stage I traffic lane should, if possible, be placed such that traffic is not allowed on top of the area where the reinforcement has been cut. See Figure 2.5.3-1. For small boxes in good condition with a skew < 30 degrees, a temporary support will not be required as long as the traffic is kept away from the edge. For concrete boxes that have skews greater than 30 degrees and/or are in poor condition, a temporary support system shall be used. A temporary support shall be used if any part of the traffic lane is on top of the unstiffened portion of the slab, or if a soil retention system has been installed on top of the culvert.

Some culverts with either very large skews or with very small skews may have been designed and built with the primary reinforcement placed parallel to the centerline of roadway. See Figure 2.5.3-1. The stage removal will not involve cutting the primary reinforcement and a temporary support will in most cases not be required.


Figure 2.5.3-1

### 2.5.4 Stage Construction of New Cast-in-Place Box Culverts

Headwalls are required at stage construction lines for most new cast-in-place culverts. They are typically one foot wide and extend nine inches above the top slab of the culvert. See Figure 2.5.4-1.

An economical choice for smaller fills is a taller-than-normal headwall. An example of this is shown in Figure 2.5.4-1. The tall headwall acts as a retaining wall at the stage line.

The headwalls at the Stage Construction line may be eliminated if the headwall is either not feasible due to clearance problems with the pavement or if the Stage II traffic lane can be moved far enough away from the Stage I Construction line to keep traffic away from the unstiffened edge. This is similar to the limitations for Stage I Traffic found in Section 2.5.2. The reinforcement bars placed in Stage I Construction are spliced to the bars in Stage II Construction with bar splicers. All bars in the slab are spliced; both longitudinal and primary bars. See Figure 2.5.4-1. This is a practical detail for culverts with little or no skew, or for skewed culverts where the main reinforcement is placed parallel to the stage construction line. However, this detail should be avoided for large skew culverts with the reinforcement placed perpendicular to the sidewalls because the formwork and bar splicer assembly placement at the stage line will become very complicated and time consuming.


Figure 2.5.4-1

For projects where the fill height is such that the Stage II Traffic limitations cannot be met with a 1:1 slope, a geotextile retaining wall or a temporary soil retention system can be built to retain the soil on top of the box as shown in Figure 2.5.4-2. While there is no minimum height for a geotextile retaining wall, a cost analysis will usually show that these types of soil retention systems are economical for larger fill heights.

Geotextile retaining walls require a minimum of 4 ft .6 in . from the Stage I Construction line to the Stage II traffic line. See Figure 2.5.4-2. A separate pay item is required when geotextile retaining walls are used. The planner should consult with their District's construction staff to discuss the amount of room that will be necessary to properly build the pavement in Stage I. In particular, clearance must be provided to allow for formwork or for equipment access along the side of the pavement and to prevent undermining. See Section 3.13.2 of the Bridge Manual for additional information and required details.

(Looking Upstation)


> STAGE I CONSTRUCTION GEOTEXTILE RETAINING WALL

Figure 2.5.4-2

### 2.5.5 Stage Construction of Precast Box Culverts

Precast concrete box culverts do not have headwalls at stage construction lines.

The typical precast concrete box culvert segment is rectangular in shape and, for a skewed crossing, the end of the segment will not be parallel to the centerline of the roadway. This leads to a loss of stage II traffic lane widths. This could require additional culvert length to accommodate temporary widening and could have an impact on the extent of right of way purchase.

### 2.6 TSL Checklist

## General

1. Check correspondence file, Bridge Condition Report, Structure Report, Structure Geotechnical Report, and Hydraulic Report to see that the TSL plan agrees with the listed reports and that the structure fits the site conditions.

## Title Block

1. Label the page as "General Plan and Elevation"
2. List the following data:
a. Roadway name/marked route over feature.
b. Designated funding route and section number.
c. County.
d. Station at the center of the structure.
e. Structure number. (New structure numbers are issued for bridges that do not reuse any part of the existing structure.)

## Location Sketch

1. Provide a sketch that shows four sections of the township.
2. Label the range, township and principle meridian.
3. Provide a north arrow.
4. Call out the structure location.
5. Check names of major features on sketch.

## Highway Classification

1. List the following data:
a. Designated funding route and roadway name/marked route.
b. Functional Class from the Illinois Structure Information System.
c. ADT - Present and Future.
d. DHV - Future.
e. ADTT \% (including single and multiple unit trucks).
f. Design speed.
g. Posted speed.

## Loading (truck)

1. Provide the correct truck loading based on the design specification.
2. Show an allowance for Future Wearing Surface (FWS).
3. On rehabilitation projects, verify the structure can support the proposed future wearing surface and meet the required rating.

## Design Specifications

1. Provide the applicable bridge design specifications.

## Design Stresses

1. Provide the design stresses for Field and Precast units.
2. Provide a separate table for design stresses of existing elements that will be incorporated into new construction.
3. Verify the correct design stresses are shown for the proposed design method.

## Upper Left Hand Corner Data

1. Provide a benchmark that matches the structure report and survey data.
2. Provide the existing structure number with the construction year and project name.
3. Provide a brief description of the existing structure.
4. Indicate the proposed method of traffic control for the proposed structure construction.
5. Indicate if any items of the existing bridge construction will be salvaged for future IDOT use.
6. Add a note stating "Precast alternate is not allowed" if site conditions require a cast-inplace culvert.

## Waterway Information Table

1. Verify the numbers match the approved hydraulic waterway information table.
2. Verify the design high water elevation matches the elevation shown in the elevation view.

## Profile Grade

1. Provide a profile grade that extends beyond the limits of the structure.
2. Show grade slopes, curve length, elevation and stations of PVC, PVT, \& PVI.
3. Verify the profile grade matches the plan and profile sheet.
4. Indicate the roadway and location of the profile grade line.

## Horizontal Curve Data

1. Provide horizontal curve data including the PI station, $\Delta, \mathrm{D}, \mathrm{R}, \mathrm{L}, \mathrm{T}, \mathrm{E}, \mathrm{PC}$ station, PT station, and SE.
2. Indicate superelevation and/or normal crown transition stations if the structure is located within a transition.

## Section Through Barrel of Structure

1. Show size of barrel opening.
2. Show thickness of walls.
3. Show thickness of top slab.
4. For cast-in-place culverts, show bottom culvert slab 1 in. thicker than top slab.
5. Indicate culvert top and bottom slab thickness is subject to refinement during final
design.
6. If there is no fill on the CIP culvert, provide corbels.
7. Show construction joints 6 in . above the top of bottom slab for CIP culverts.
8. Show construction joints between walls and top slab for CIP culverts.
9. Indicate Phoebe nesting sites at downstream end of interior walls on CIP culverts.
10. The top and bottom slabs of multiple cell box culvert extensions should be designed as continuous members according to present design policies.

## Longitudinal Section

1. Show lane, shoulder, median, barrier, and sidewalk widths.
2. Show roadway cross slopes.
3. Show profile grade location.
4. Show guardrail (if required)
a. Verify guardrail placement behind curb (BD\&E Manual Chapter 38)
b. Verify slope "hinge point" is 3 ft - 10 in . min. from face of guardrail (See Hwy. Std. 630001).
c. If attaching guardrail to culvert, reference either Hwy. Std. 630001 or 630111. If guardrail will span culvert, reference Hwy. Std. 630106.
5. Show height of barriers and pedestrian rails.
6. Show upstream and downstream flow-line and invert elevations. (Set invert 3 in. below flow-line.)
7. Show design high-water elevation (at upstream end of culvert) and EWSE.
8. Show height and width of headwall.
9. Show stage traffic widths.
10. Show stage construction widths.
11. Verify stage construction is consistent with condition of existing bridge (and the District's desire).
12. Show temporary concrete barrier.
13. Show top and bottom slab thickness.
14. Verify the need for an edge beam on the top slab of cast-in-place culverts at the stage construction joint. (Note, an edge beam is typically not required if stage traffic is located further than half of the design live load distribution width from the stage construction joint.)
15. Show cutoff walls depth.
16. Show buried utilities
17. Plot natural ground line.

## Plan View

1. Show dimension from out-to-out of headwalls (i.e. length along walls).
2. Show controlling culvert dimensions perpendicular to barrels.
3. Show approach roadway template.
4. Give skew angle.
5. Show width of headwall.
6. Show typical value of side-slopes in vicinity of culvert wingwalls.
7. Show station and elevation on profile grade at CL of culvert.
8. Show culverts with stationing increasing to the top of the page.
9. Show flow direction under roadway.
10. Show CL of culvert.
11. Indicate and check important horizontal clearances.
12. Show stage construction line and locate on roadway.
13. Show temporary construction details (sheet piling, geotextile wall, etc.) when applicable.
14. Show limits of existing structure.
15. Plot boring locations.
16. Show pipe culverts and local drainage near structure.
17. Show bridge approach slab if there is no fill on the culvert.
18. Show guardrail.
19. Show type of curb and gutter.
20. Show north arrow.

## Stream Protection Details

1. Verify the need for stream protection (i.e. riprap, aprons, etc.) and show stream protection details as required.

### 2.7 Example Type, Size, and Location Reports

TSL Ex. 14 Straight Highway over Creek

- Two Barrel Box Culvert (Embankment Fill on Top Slab)

TSL Ex. 15 Straight Highway over Creek

- Three Barrel Box Culvert (No Embankment Fill on Top Slab)


## Section 3 Design

This design section of the Culvert Manual provides guidance for cast-in-place concrete box culverts. The intent of IDOT culvert design policy is to design concrete box culverts in accordance with the AASHTO LRFD Bridge Design Specifications with few deviations. Designers should familiarize themselves with Chapter 12 of the design specifications prior to beginning their work.

### 3.1 Design Codes

The structural design of a new box culvert shall be in accordance with the specification shown on the approved Type, Size, and Location Report (TSL). If a TSL has not been prepared, the design shall be in accordance with the current edition of the AASHTO LRFD Bridge Design Specifications.

The structural design of widening of an existing box culvert shall be consistent with the design method used in the original design.

- Extensions of box culverts originally designed according to either the service load design method (ASD) or load factor design (LFD) method shall be designed using the load factor design (LFD) method according to the AASHTO Standard Specifications for Highway Bridges $17^{\text {th }}$ Edition 2002.
- Extensions of box culverts, where the existing culvert was originally designed according to any edition of the AASHTO LRFD Bridge Design Specifications, shall be designed according to current edition of the AASHTO LRFD Bridge Design Specifications.


### 3.2 Load Combinations

As per Article C12.11.2 of the AASHTO LRFD Bridge Design Specifications, concrete box culverts shall be designed for the following Strength I load combinations.

Strength I maximum vertical load and maximum horizontal load:

$$
\left.\eta\left[(1.25) \mathrm{DC}+(1.5) \mathrm{DW}+(1.30) \mathrm{EV}+(1.75)(\mathrm{LL}+\mathrm{IM})+(1.35) \mathrm{EH}_{\max }+(1.50) \mathrm{ES}_{\max }+(1.75) \mathrm{LS}\right)\right]
$$

Strength I maximum vertical load and minimum horizontal load:

$$
\eta[(1.25) \mathrm{DC}+(1.5) \mathrm{DW}+(1.30) \mathrm{EV}+(1.75)(\mathrm{LL}+\mathrm{IM})]+(1 / \eta)\left[(0.9) \mathrm{EH}_{\min }+(0.75) \mathrm{ES}_{\min }\right]
$$

Strength I minimum vertical load and maximum horizontal load:

$$
(1 / \eta)[(0.90) \mathrm{DC}+(0.90) \mathrm{EV}]+\eta\left[(1.35) \mathrm{EH}_{\max }+(1.75) \mathrm{LS}\right]
$$

Load modifiers ( $\eta$ factors) are given in Section 3.3 below. As per Article 1.3.2 of the AASHTO LRFD Bridge Design Specifications, for maximum load effects, the $\eta$ factors are applied to the loads. For minimum load effects, a factor equal to the inverse of $\eta$ is applied to the loads.

For serviceability checks, the following load case is applied. Note that $\eta$ factors are not applicable to serviceability checks.

Service I vertical load and horizontal load:

$$
1.00 \mathrm{DC}+1.00 \mathrm{DW}+1.00 \mathrm{EV}+1.00(\mathrm{LL}+\mathrm{IM})+1.00 \mathrm{EH}_{\max }+1.00 \mathrm{ES}_{\max }+1.00 \mathrm{LS}
$$

DC, DW, EV, LL, IM, EH, ES, and LS are load types, defined in Chapter 3 of the AASHTO LRFD Bridge Design Specifications and further clarified in this manual.

As per Article 5.5.3.1 of the AASHTO LRFD Bridge Design Specifications, reinforced concrete box culverts need not be analyzed for fatigue.

According to Article 3.10.1 of the AASHTO LRFD Bridge Design Specifications, buried structures are not designed for seismic effects. Wingwalls and retaining walls adjacent to culverts are considered parts of the buried structures. As such, they also are not designed for the seismic loading effects given in Articles 11.5.4 and 11.6.5 of the AASHTO LRFD Bridge Design Specifications, regardless of the adjusted peak ground acceleration (PGA) or liquefaction concerns.

### 3.3 Load Modifiers

The following load modifiers $\eta$ for ductility, redundancy and operational classification shall be applied to the Strength I load combination force effects for all box culverts:

- $\eta_{d}=1.0$ for ductility
- $\eta_{r}=1.05$ for redundancy
- $\quad \eta_{I}=1.0$ for operational importance, for culverts with fill heights less than 15 feet
- $\eta_{\mathrm{I}}=1.05$ for operational importance, for culverts with fill heights greater than or equal to 15 feet


### 3.4 Loads

Loads and live load distribution shall be in accordance with Article 12.11.2 of the AASHTO LRFD Bridge Design Specifications except as noted.

### 3.4.1 Fill Height

The fill height used in the determination of the live load distribution shall be the difference in elevation between the top of the pavement and the top of the top slab. The thickness of the Future Wearing Surface on the calculation of fill height shall be ignored.

For culvert design purposes, the roadway width is defined as the distance from one outside edge of paved shoulder to the outside edge of the other paved shoulder. The design fill heights shall be the maximum and minimum fill heights calculated within this distance. See Figure 3.4.1-1. Fill heights may be rounded to the nearest foot. The controlling fill condition shall be used for the design of the entire culvert. For culverts with a maximum fill height less than 5 feet, the lesser fill height will most likely control.


## FILL HEIGHT

Figure 3.4.1-1

For culverts where the fill height varies by over ten feet, portions of the culvert may be designed for differing fill heights, subject to coordination and concurrence with the Bureau of Bridges and Structures.

### 3.4.2 Dead Load- DC

For the calculation of concrete dead loads, the unit weight of reinforced concrete $\left(\gamma_{c}\right)$ shall be 150 pcf.

Unless otherwise specified on the TSL Report, a 12 in. thick pavement and shoulder shall be assumed to be present for the purpose of load calculation. The unit weight of the pavement shall be assumed to be 150 pcf for both concrete and asphalt pavement.

### 3.4.3 Future Wearing Surface- DW and ES

Unless otherwise specified on the TSL Report, a future wearing surface with a weight of 50 psf shall be assumed to be present. The presence of a future wearing surface shall not be assumed to be fill and shall not be used to change the assumed live load distribution. For the purpose of design, DW shall be considered to be a surcharge load (ES) on the culvert.

### 3.4.4 Vertical Earth Pressure- EV

Vertical earth pressure shall be calculated assuming an embankment installation. See Article 12.11.2.2 of the AASHTO LRFD Bridge Design Specifications. Unless otherwise specified on the TSL Report, the unit weight of soil on top of the box culvert $\left(\gamma_{\mathrm{s}}\right)$ shall be assumed to be 120 pcf.

For the purpose of determining the load factor from Table 3.4.1-2 of the AASHTO LRFD Bridge Design Specifications, box culverts with pinned corners, which is the standard IDOT model for cast-in-place culverts, are considered rigid buried structures. Trench installation and positive projection may not be used to reduce loads on the culvert due to incompatibility with the IDOT Standard Specifications for Road and Bridge Construction and normal construction techniques.

### 3.4.5 Horizontal Earth Pressure- EH, Earth Surcharge- ES, Live Load Surcharge- LS

Figure 3.4.5-1 illustrates the load application of horizontal earth pressure (EH), earth surcharge (ES), and live load surcharge (LS).

The horizontal earth pressure (EH) on the culvert sidewalls shall be calculated assuming at rest conditions with earth pressure coefficient $k_{0}$ equal to 0.5 . The unit weight of backfill shall be assumed to be 120 pcf, which results in an equivalent fluid pressure of 60 pcf. Note that this is a significant increase from past specifications and will result in higher forces in sidewalls.

The minimum horizontal earth pressure shall be $50 \%$ of the maximum pressure in accordance with Article 3.11.7 of the AASHTO LRFD Bridge Design Specifications.

The backfill shall be assumed to be drained for dry conditions and wet conditions. The effects of water (WA) may be ignored in load calculations.

Earth surcharge (ES) is added in non-zero fill conditions. It is a rectangular load based on the equivalent fluid pressure and the fill height.

Live load surcharge (LS) shall be applied to all culverts regardless of fill height and shall be calculated according to Article 3.11.6.4 of the AASHTO LRFD Bridge Design Specifications. The fill height of soil used in LS calculations shall be the same as that used in EV calculations.
Table 3.11.6.4-1 Equivalent Height of Soil for Vehicular Loadings on Abutments Perpendicular to Traffic found in the AASHTO LRFD Bridge Design Specifications shall be used for culverts of all skews.


Figure 3.4.5-1

### 3.4.6 Live Load Plus Impact - LL+IM

Live load shall be determined according to Article 3.6.1.3.3 of the AASHTO LRFD Bridge Design Specifications. For the purpose of interpretation of this article relative to when live load effects can be neglected, the term "span length" may be interpreted as "clear span". For example, a single $8 \times 6$ box culvert with 8.1 feet of fill need not be designed for live load. Likewise, for the design of multiple barrel box culverts, the effects of live load may be neglected when the fill height is greater than the distance between the inside faces of the exterior walls. Loading for single box culverts shall be from one vehicle and a Multiple Presence Factor of 1.2 shall be applied. The past practice of calculating loads produced by side by side trucks has been discontinued in the AASHTO LRFD Bridge Design Specifications. Lane load is not considered in the design of box culverts.

Live load is distributed to the culvert over an area determined by one of two methods. For culverts with less than two feet of fill (contact loading), the load is distributed over an area determined using provisions in Article 4.6.2.10 of the AASHTO LRFD Bridge Design Specifications. For culverts with fills two feet in height or greater, the load is distributed through the fill using the provisions of Article 3.6.1.2.6b of the AASHTO LRFD Bridge Design Specifications, using a distribution factor of 1.15.

Article 3.6.1.2.6 states that if the moments caused by distributing wheel or axle loads through fill exceed those caused by contact loading, the moments caused by contact loading shall be used. For smaller fills, this may result in contact loading being used in lieu of distributing the load through the fill, even though the force effects due to contact loading are less.

To simplify calculations when distributing load through fills, the live load patch for the design truck or tandem may be taken as the combination of both wheels for trucks or all four wheels for tandems. The assumption of one larger patch load with a lesser intensity results in higher moments than the assumption of two smaller patch loads with greater intensity. See Figure 3.4.6-1 for more information.

Impact shall be calculated according to Article 3.6.2.2 of the AASHTO LRFD Bridge Design Specifications.

The past practice of ignoring distribution of live load in the direction of movement for fills $<2$ feet is discouraged. Whereas the requirement to check shear in culverts with fills $<2$ feet was not in the AASHTO Standard Specifications for Highway Bridges, the LRFD Specifications require shear be checked. Shear may control the design of top slab thickness for culverts with shallow fills. Distributing the load in the direction of movement will reduce the calculated shear forces and allow for slabs thinner than those found if determined by assuming point loads.

For single box culverts, the effects of skew are not considered unless traffic is moving perpendicular to the span, i.e. a 90 degree skew. For multiple box culverts, the effects of skew shall be considered when the skew exceeds 30 degrees.

When the effect of skew is considered, the culvert shall be designed for traffic travelling parallel to the span and traffic travelling perpendicular to the span. The provisions of Article 4.6.2.1 of the AASHTO LRFD Bridge Design Specifications shall be used for the condition of traffic moving perpendicular to the span.

$$
\begin{aligned}
& l_{p}=10^{\prime \prime}+1.15 F \\
& l_{t}=6^{\prime}+20^{\prime \prime}+1.15 F
\end{aligned}
$$



DISTRIBUTING LOAD
THROUGH FILLS
Figure 3.4.6-1

### 3.5 Design

All components shall be designed for flexure, serviceablility, and shear. Detailing requirements, consisting of minimum and maximum reinforcement areas and spacings also apply.

All reinforcement shall have a clear cover of two inches. This increase in clear cover is intended to provide additional durability.

Epoxy-coated reinforcement shall be used in all portions of concrete box culverts with zero-fill situations.

### 3.5.1 Material Properties

Unless otherwise approved by the Bureau of Bridges and Structures, material properties shall be as follows:

| Concrete Unit Weight $\gamma_{c}$ (for calculation of $\mathrm{E}_{\mathrm{c}}$ ) | 145 pcf |
| :--- | :---: |
| Concrete Unit Weight $\gamma_{\mathrm{c}}$ (for load calculations) | 150 pcf |
| Concrete Compressive Strength, $\mathrm{f}_{\mathrm{c}}$ | 3.5 ksi |
| Reinforcement Bars Yield Strength, $\mathrm{f}_{\mathrm{y}}$ | 60 ksi |
| Modulus of Elasticity of Concrete, $\mathrm{E}_{\mathrm{c}}$ | See AASHTO LRFD |
| Modular Ratio, n | Eq. $5.4 .2 .4-1$ |
|  | $29000 \mathrm{ksi} / \mathrm{E}_{\mathrm{c}}$ |

### 3.5.2 Modeling, Reinforcement Orientation, and Design Span

Top and bottom slabs of cast-in-place concrete box culverts shall be considered to be pinned at the centerline of all adjacent walls.

For multi-span culverts, the critical section for moment at interior supports may be taken at the face of the interior wall. However, it is simpler and more conservative to take it at the centerline of the interior wall, which is also acceptable.

For the purpose of determining forces in sidewalls, the design span shall be assumed to be the distance from the center of the top slab to the center of the bottom slab. The sidewalls shall be considered to be pinned to the top and bottom slabs at these locations.

For culverts without stage construction, main reinforcement in top and bottom slabs shall be placed perpendicular to the sidewalls, and the design span shall be assumed to be the center-to-center distance from one support to the next support, measured perpendicular to sidewalls.

For culverts with stage construction and skews less than 50 degrees, main reinforcement in top and bottom slabs shall be placed parallel to the headwalls. The design span for these culverts shall be assumed to be the center-to-center distance from one support to the next support measured perpendicular to the sidewalls. The amount of main reinforcement required for this design span shall then be multiplied by the secant squared of the skew ( $\sec ^{2}$ (skew angle)), and the resulting amount of reinforcement shall be placed in the culvert.

For culverts with stage construction and skews greater than or equal to 50 degrees, main reinforcement in top and bottom slabs shall be placed parallel to the headwalls. The design span for these culverts shall be assumed to be the center-to-center distance from one support to the next support measured parallel to the headwall.

See Fig. 3.5.2-1 for additional details.

If the amount of reinforcement required for highly skewed culverts with stage construction becomes excessive, the main reinforcement may be placed perpendicular to supports, with the design span measured perpendicular to supports. This often results in difficult formwork and reinforcement placement along the stage construction line and is discouraged.


STAGE CONSTRUCTION SKEWS $\geq 50^{\circ}$

Figure 3.5.2-1

### 3.5.3 Geometric Requirements

For concrete placement purposes, the minimum allowable thickness of a wall or slab with one mat of reinforcement shall be six (6) inches. The minimum allowable thickness of a wall with two mats of reinforcement shall be ten (10) inches.

The minimum thickness of a slab in inches shall be equal to the clear span in feet. The minimum thickness of a wall in inches shall be equal to the clear height in feet.

The thickness of the bottom slab shall be one inch greater than the thickness of the top slab for cast-in-place culverts.

### 3.5.4 Flexural Resistance

To satisfy ultimate strength requirements, flexural resistance shall be calculated in accordance with Article 5.7.3.2 of the AASHTO LRFD Bridge Design Specifications.

The resistance factor for combined flexure and axial load shall be in accordance with Article 5.5.4.2 and Equation 5.5.4.2.1-2 of the AASHTO LRFD Bridge Design Specifications. The provisions of Article 12.5 .5 shall not be used.

To simplify calculations, axial loads may be conservatively ignored. However, it may be advantageous to consider axial load effects.

### 3.5.5 Control of Cracking by Distribution of Reinforcement

To satisfy serviceablility requirements, reinforcement spacing shall satisfy the crack control requirements of Article 5.7.3.4 of the AASHTO LRFD Bridge Design Specifications.

The reinforcement bar stress at the Service I limit state shall be limited to 36 ksi .

The exposure factor, $\gamma_{\mathrm{E}}$, shall be taken as 0.75 for all concrete box culverts.

While not recommended due to the additional complexity, the provisions of C12.11.3 of the AASHTO LRFD Bridge Design Specifications may be used to account for the influence of axial load on the service stress. For determining stresses in the sidewall, the axial load, $\mathrm{N}_{\mathrm{s}}$, shall be calculated assuming the embankment factor, $\mathrm{F}_{\mathrm{e}}$, is equal to 1.0 . For determining stresses in the top or bottom slab, $\mathrm{N}_{\mathrm{s}}$ shall be calculated assuming the equivalent horizontal earth pressure (EH) is one-half of the design pressure and the contribution from live load surcharge (LS) is zero.

### 3.5.6 Limitation on Maximum Reinforcement

All reinforced concrete shall be either tension controlled or in the transition zone as noted in Article 5.5.4.2 and Figure C.5.5.4.2.1-1 of the AASHTO LRFD Bridge Design Specifications. For routine designs, maximum reinforcement in box culvert top slabs and sidewalls should be limited to $0.375 \rho_{\text {bal }}$ where $\rho_{\text {bal }}$ is calculated using the following equation:

$$
\rho_{\text {bal }}=\frac{0.85 \beta_{1} f_{c}}{f_{y}}\left(\frac{87000}{87000+f_{y}}\right)
$$

For non-routine design, such as the case where minimizing top slab thickness is required to provide minimum cover over the culvert in low-fill situations, $\rho$ may be increased to $0.6 \rho_{\text {bal }}$. This will provide that the flexural capacity at the balance point is greater than the flexural capacity at zero axial load.

The past practice of proportioning slabs for minimum thickness is discouraged. A marginal increase in slab thickness can result in a significant reduction in the amount of reinforcement and reduce the overall cost of the culvert.

### 3.5.7 Limitation on Minimum Reinforcement

All culvert slabs and sidewalls shall be reinforced to develop a minimum factored resistance equal to the lesser of 1.33 times the factored moment required by the applicable strength load combination specified in Table 3.4.1-1, or the cracking moment $\mathrm{M}_{\mathrm{cr}}$, as determined by Eq. 5.7.3.3.2-1 of the AASHTO LRFD Bridge Design Specifications.

### 3.5.8 Maximum Reinforcement Spacing

Reinforcement spacing shall be in accordance with Article 5.7.3.4 of the AASHTO LRFD Bridge Design Specifications, except the maximum spacing for primary flexural reinforcement shall be limited to 12 inches. For determination of crack control requirements, the exposure condition shall be assumed to be Class 2, with $\gamma_{E}=0.75$.

The requirements of Article 5.10.3.2 of the AASHTO LRFD Bridge Design Specifications shall be satisfied.

### 3.5.9 Minimum Reinforcement Spacing

The minimum spacing for primary flexural reinforcement shall be 5 inches. When bar laps are used, the minimum clear distance between the adjacent lapped bars shall not be less than 4 inches.

### 3.5.10 Bar Size Limitations

The minimum size of reinforcement used in a cast-in-place concrete box culvert shall be 0.5 in . diameter (\#4) reinforcement.

The reinforcement bar sizes shown in Table 3.5.10-1 were used in development of the singlespan culvert standard design tables. Use of this table will aid in preliminary design.

| Slab Thickness <br> (inches) | Max Bar Size |
| :---: | :---: |
| 6 | 5 |
| $7 \leq \mathrm{t}<10$ | 6 |
| $10 \leq \mathrm{t}<12$ | 7 |
| $12 \leq \mathrm{t}<15$ | 8 |
| $15 \leq \mathrm{t}<18$ | 9 |
| $\mathrm{t} \leq 18$ | $11^{*}$ |

Table 3.5.10-1
*While \#11 bars may be used in thick slabs, the preferred maximum bar size is \#9. Slabs thicker than 20 " may require two layers of reinforcement to satisfy this preference.

### 3.5.11 Distribution, Temperature, and Shrinkage Reinforcement

Distribution reinforcement shall be provided for all reinforcement bars required for strength. The amount of reinforcement required shall be calculated using the provisions of Article 5.14.4.1 of the AASHTO LRFD Bridge Design Specifications. The maximum spacing of distribution reinforcement shall be 12 inches. The recommended maximum reinforcement size for longitudinal reinforcement is 0.875 in . (\#7) reinforcement. Longitudinal reinforcement bars shall not be larger in diameter than the primary flexural reinforcement. Class B laps shall be used for longitudinal reinforcement.

For culverts with fills less than two (2) feet, slabs with thicknesses greater than or equal to eight (8) inches, or walls with thicknesses greater than or equal to ten (10) inches, temperature and shrinkage reinforcement shall be provided for both inside and outside faces of culvert walls. For all other cases, temperature and shrinkage reinforcement is only required to be provided on the exposed face of the wall or slab. The amount of temperature reinforcement required shall be calculated using the provisions of Article 5.10.8 of the AASHTO LRFD Bridge Design Specifications.

See Figures 3.5.11-1 and 3.5.11-2 for more details.


TOP SLAB SECTION - A
Fill Height $<2^{\prime}-0^{\prime \prime}$ or $T \geq 8^{\prime \prime}$


$$
\frac{\text { TOP SLAB SECTION }-B}{\text { Fill Height } \geq 2^{\prime}-0^{\prime \prime} \& T<8^{\prime \prime}}
$$

## NOTE:

Number of h bars
in top slab includes 2bars in top of the slab as shown.


* Provide $2^{\prime} 4^{\prime \prime} \mathrm{cl} . \pm^{\prime \prime \prime}$ when fill on top slab is zero, and epoxy coat bars in top slab.

a 1 BARS
Top slab shown, bottom slab similar
For dimensions $A$ and $B$, see Table 5.1-1

> TOP AND BOTTOM

SLAB DETAILS

Figure 3.5.11-1


* See Table 5.1-2 for required lap length

SIDEWALL DETAILS

Figure 3.5.11-2

### 3.5.12 Shear Capacity

The resistance factor for shear shall be in accordance with Article 12.5 .5 of the AASHTO LRFD Bridge Design Specifications.

For culverts top slabs with fill height of 2 feet or greater, the flexural reinforcement bar size shall preferably be sized and detailed such that the bar is fully developed on both sides of the critical section. If the reinforcement is not fully developed, the area of steel $A_{s}$ in Eq. 5.14.5.3-1 of the AASHTO LRFD Bridge Design Specifications shall be proportionally reduced by an amount equal to the ratio of the actual length provided to the length required for full development. This is consistent with the shear capacity provisions for culvert top slabs with fill height less than 2 feet and for culvert sidewalls.

The shear capacity lower limit provision of Article 5.14 .5 . 3 for simply supported slabs, $0.0791 \sqrt{f^{\prime}}{ }_{c}$ bd , shall apply only if the reinforcement is fully developed on both sides of the critical section.

### 3.6 Standard Design Tables for Single-Box Cast-in-Place Concrete Culverts

Standard design tables for single-box cast-in-place concrete culverts are given below. To utilize these tables, the maximum and minimum fill heights shall be calculated as per Figure 3.4.1-1. Fill heights may be rounded to the nearest foot. The controlling fill height is the height that results in the maximum required concrete volume.

Example:

4' $\times 3$ ' single-box cast-in-place culvert

Maximum fill height $=4 \mathrm{ft}$.

As per table, required concrete volume $=0.343 \mathrm{cu} . \mathrm{yd} . / \mathrm{ft}$.

Minimum fill height $=1 \mathrm{ft}$.

As per table, required concrete volume $=0.404 \mathrm{cu} . \mathrm{yd} . / \mathrm{ft}$.

Use reinforcement and member thicknesses corresponding to 1 ft . of fill.

3' CLEAR SPAN BY 2' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1} \mathrm{BAR}$ |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { T } \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 8 | A | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.284 |
| 1 | 8 | A | 5 | 5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.284 |
| 2 | 8 | A | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.284 |
| 3 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.235 |
| 4 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.235 |
| 5 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.235 |
| 6 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.235 |
| 7 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.235 |
| 8 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.235 |
| 9 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.235 |
| 10 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.235 |
| 11 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.235 |
| 12 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.235 |
| 13 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.235 |
| 14 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.235 |
| 15 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.235 |
| 20 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.259 |
| 25 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.259 |


| 3' CLEAR SPAN BY 3' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  |  |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 8 | A | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.321 |
| 1 | 8 | A | 5 | 5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.321 |
| 2 | 8 | A | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.321 |
| 3 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.272 |
| 4 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.272 |
| 5 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.272 |
| 6 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.272 |
| 7 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.272 |
| 8 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.272 |
| 9 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.272 |
| 10 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.272 |
| 11 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.272 |
| 12 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.272 |
| 13 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.272 |
| 14 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.272 |
| 15 | 6 | B | 4 | 5.5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.272 |
| 20 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.296 |
| 25 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.296 |

4' CLEAR SPAN BY 2'CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. $3 / \mathrm{ft}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { FILL } \\ \mathrm{ft.} \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 8.5 | A | 5 | 5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.352 |
| 1 | 9 | A | 5 | 5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.367 |
| 2 | 9 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.367 |
| 3 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.306 |
| 4 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.306 |
| 5 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.306 |
| 6 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.306 |
| 7 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.306 |
| 8 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.306 |
| 9 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.306 |
| 10 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.306 |
| 11 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.306 |
| 12 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.306 |
| 13 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.306 |
| 14 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.321 |
| 15 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.321 |
| 20 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.321 |
| 25 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.352 |


| 4' CLEAR SPAN BY 3' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v B A R$ |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| $\begin{array}{\|c} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{array}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 8.5 | A | 5 | 5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.389 |
| 1 | 9 | A | 5 | 5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.404 |
| 2 | 9 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.404 |
| 3 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.343 |
| 4 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.343 |
| 5 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.343 |
| 6 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.343 |
| 7 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.343 |
| 8 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.343 |
| 9 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.343 |
| 10 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.343 |
| 11 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.343 |
| 12 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.343 |
| 13 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.343 |
| 14 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.358 |
| 15 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.358 |
| 20 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.358 |
| 25 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.389 |

4' CLEAR SPAN BY 4' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \mathrm{SIZE} \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{aligned} & \text { SPC. } \\ & \text { in. } \end{aligned}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 8.5 | A | 5 | 5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.426 |
| 1 | 9 | A | 5 | 5 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.441 |
| 2 | 9 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.441 |
| 3 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.38 |
| 4 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.38 |
| 5 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.38 |
| 6 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.38 |
| 7 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.38 |
| 8 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.38 |
| 9 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.38 |
| 10 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.38 |
| 11 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.38 |
| 12 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.38 |
| 13 | 7 | B | 5 | 7 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.38 |
| 14 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.395 |
| 15 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.395 |
| 20 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.395 |
| 25 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7.5 | 4 | 12 | 0.46 |


| 5' CLEAR SPAN BY 2' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $h_{1}$ BAR |  | WALL |  | $v B A R$ |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| $\begin{array}{\|c} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{array}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 9.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.444 |
| 1 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.426 |
| 2 | 9.5 | A | 6 | 5.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.444 |
| 3 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.37 |
| 4 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.37 |
| 5 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.37 |
| 6 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.37 |
| 7 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.37 |
| 8 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.37 |
| 9 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.37 |
| 10 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.37 |
| 11 | 8 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.389 |
| 12 | 8 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.389 |
| 13 | 8 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.389 |
| 14 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.407 |
| 15 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.407 |
| 20 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.444 |
| 25 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.463 |

5' CLEAR SPAN BY 3' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v B A R$ |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|c} \hline \text { FILL } \\ \mathrm{ft.} . \end{array}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in } \end{aligned}$ | SEC. | $\begin{array}{c\|} \hline \text { SIZE } \\ \# \end{array}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 9.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.481 |
| 1 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.463 |
| 2 | 9.5 | A | 6 | 5.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.481 |
| 3 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.407 |
| 4 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.407 |
| 5 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.407 |
| 6 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.407 |
| 7 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.407 |
| 8 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.407 |
| 9 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.407 |
| 10 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.407 |
| 11 | 8 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.426 |
| 12 | 8 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.426 |
| 13 | 8 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.426 |
| 14 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.444 |
| 15 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.444 |
| 20 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.481 |
| 25 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.5 |


| 5' CLEAR SPAN BY 4' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  |  |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { T } \\ \text { in. } \\ \hline \end{array}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{array}{\|l} \hline \text { W } \\ \text { in. } \\ \hline \end{array}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SIZE } \\ \# \\ \hline \end{array}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 9.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.519 |
| 1 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.5 |
| 2 | 9.5 | A | 6 | 5.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.519 |
| 3 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.444 |
| 4 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.444 |
| 5 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.444 |
| 6 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.444 |
| 7 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.444 |
| 8 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.444 |
| 9 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.444 |
| 10 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.444 |
| 11 | 8 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.463 |
| 12 | 8 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.463 |
| 13 | 8 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.463 |
| 14 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.481 |
| 15 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.481 |
| 20 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.519 |
| 25 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7.5 | 4 | 12 | 0.573 |

5' CLEAR SPAN BY 5' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1} \mathrm{BAR}$ |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v B A R$ |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 9.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.556 |
| 1 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.537 |
| 2 | 9.5 | A | 6 | 5.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.556 |
| 3 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.481 |
| 4 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.481 |
| 5 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.481 |
| 6 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.481 |
| 7 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.481 |
| 8 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 5 | 7.5 | 4 | 12 | 0.481 |
| 9 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 5 | 7.5 | 4 | 12 | 0.481 |
| 10 | 7.5 | B | 5 | 6 | 4 | 12 | 4 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.481 |
| 11 | 8 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.5 |
| 12 | 8 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.5 |
| 13 | 8 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.52 |
| 14 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.539 |
| 15 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.559 |
| 20 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 7 | A | 5 | 6 | 4 | 12 | 0.597 |
| 25 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.657 |


| 6' CLEAR SPAN BY 2' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | h, BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  | Conc. <br> Vol. yd. 3 / ft |
| $\begin{array}{\|c} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{array}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \\ & \hline \end{aligned}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 9.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.506 |
| 1 | 9.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.506 |
| 2 | 10 | A | 6 | 5.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.528 |
| 3 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.463 |
| 4 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.463 |
| 5 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.463 |
| 6 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.463 |
| 7 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.463 |
| 8 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.463 |
| 9 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.463 |
| 10 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.463 |
| 11 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.463 |
| 12 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.463 |
| 13 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.463 |
| 14 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.506 |
| 15 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.506 |
| 20 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.528 |
| 25 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.571 |

6' CLEAR SPAN BY 3' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1} \mathrm{BAR}$ |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{array}{\|c} \hline \text { SIZE } \\ \# \end{array}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 9.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.543 |
| 1 | 9.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.543 |
| 2 | 10 | A | 6 | 5.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.565 |
| 3 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.5 |
| 4 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.5 |
| 5 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.5 |
| 6 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.5 |
| 7 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.5 |
| 8 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.5 |
| 9 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.5 |
| 10 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.5 |
| 11 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.5 |
| 12 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.5 |
| 13 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.5 |
| 14 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.543 |
| 15 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.543 |
| 20 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.565 |
| 25 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.608 |


| 6' CLEAR SPAN BY 4' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}, \mathrm{~h}$ BAR |  | h, BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  | Conc. <br> Vol. <br> yd. ${ }^{3} / \mathrm{ft}$. |
| $\begin{array}{\|c} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{array}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \\ & \hline \end{aligned}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 9.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.58 |
| 1 | 9.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.58 |
| 2 | 10 | A | 6 | 5.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.602 |
| 3 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.537 |
| 4 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.537 |
| 5 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.537 |
| 6 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.537 |
| 7 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.537 |
| 8 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.537 |
| 9 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.537 |
| 10 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.537 |
| 11 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.537 |
| 12 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.537 |
| 13 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.537 |
| 14 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.58 |
| 15 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.58 |
| 20 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.602 |
| 25 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7.5 | 4 | 12 | 0.682 |

6' CLEAR SPAN BY 5' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 9.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.617 |
| 1 | 9.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.617 |
| 2 | 10 | A | 6 | 5.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.639 |
| 3 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.574 |
| 4 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.574 |
| 5 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.574 |
| 6 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.574 |
| 7 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.574 |
| 8 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 6 | A | 5 | 7.5 | 4 | 12 | 0.574 |
| 9 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 5 | 7.5 | 4 | 12 | 0.574 |
| 10 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.574 |
| 11 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.574 |
| 12 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.574 |
| 13 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.594 |
| 14 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.638 |
| 15 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.658 |
| 20 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 7 | A | 5 | 6 | 4 | 12 | 0.681 |
| 25 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.767 |


| 6' CLEAR SPAN BY 6' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | $\begin{gathered} \text { Conc. } \\ \text { Vol. } \\ \text { yd. }{ }^{3} / \mathrm{ft} . \end{gathered}$ |
| $\begin{array}{\|c} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{array}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 9.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.654 |
| 1 | 9.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.654 |
| 2 | 10 | A | 6 | 5.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.676 |
| 3 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 7 | A | 4 | 5.5 | 4 | 12 | 0.634 |
| 4 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7.5 | 4 | 12 | 0.634 |
| 5 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.657 |
| 6 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.657 |
| 7 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.657 |
| 8 | 8.5 | A | 6 | 7.5 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.681 |
| 9 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.681 |
| 10 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.681 |
| 11 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.681 |
| 12 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.681 |
| 13 | 8.5 | A | 6 | 7 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.681 |
| 14 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.725 |
| 15 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.749 |
| 20 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 |  | A | 6 | 7.5 | 5 | 12 | 0.796 |
| 25 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 0.866 |

7' CLEAR SPAN BY 2' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1} \mathrm{BAR}$ |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3}$ / ft. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.568 |
| 1 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.568 |
| 2 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.568 |
| 3 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.568 |
| 4 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.543 |
| 5 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.543 |
| 6 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.543 |
| 7 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.543 |
| 8 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.568 |
| 9 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.568 |
| 10 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.593 |
| 11 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.593 |
| 12 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.593 |
| 13 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.593 |
| 14 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.593 |
| 15 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.593 |
| 20 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.667 |
| 25 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.716 |


| 7' CLEAR SPAN BY 3' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v B A R$ |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. 3 / ft |
| $\begin{gathered} \mathrm{FILL} \\ \mathrm{ft} . \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SIZE } \\ \# \end{array}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.605 |
| 1 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.605 |
| 2 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.605 |
| 3 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.605 |
| 4 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.58 |
| 5 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.58 |
| 6 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.58 |
| 7 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.58 |
| 8 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.605 |
| 9 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.605 |
| 10 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.63 |
| 11 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.63 |
| 12 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.63 |
| 13 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.63 |
| 14 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.63 |
| 15 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.63 |
| 20 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.704 |
| 25 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.753 |

7' CLEAR SPAN BY 4' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1} \mathrm{BAR}$ |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \mathrm{FILL} \\ \mathrm{ft} . \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{aligned} & \text { SPC. } \\ & \text { in. } \end{aligned}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.642 |
| 1 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.642 |
| 2 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.642 |
| 3 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.642 |
| 4 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.617 |
| 5 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.617 |
| 6 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.617 |
| 7 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.617 |
| 8 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.642 |
| 9 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.642 |
| 10 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.667 |
| 11 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.667 |
| 12 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.667 |
| 13 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.667 |
| 14 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.667 |
| 15 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.667 |
| 20 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.741 |
| 25 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7.5 | 4 | 12 | 0.828 |

7' CLEAR SPAN BY 5' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { FILL } \\ \mathrm{ft.} \end{gathered}$ | $\begin{array}{\|c} \hline \mathrm{T} \\ \text { in. } \\ \hline \end{array}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \\ \hline \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \\ \hline \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c\|} \hline \mathrm{SPC} . \\ \text { in. } \end{array}$ | $\begin{array}{\|l\|} \hline \text { W } \\ \text { in. } \end{array}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.679 |
| 1 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.679 |
| 2 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.679 |
| 3 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.679 |
| 4 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.654 |
| 5 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.654 |
| 6 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.654 |
| 7 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.654 |
| 8 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 5 | 7.5 | 4 | 12 | 0.679 |
| 9 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 5 | 7.5 | 4 | 12 | 0.679 |
| 10 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.704 |
| 11 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.704 |
| 12 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.704 |
| 13 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.725 |
| 14 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.725 |
| 15 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.745 |
| 20 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 7 | A | 5 | 6 | 4 | 12 | 0.821 |
| 25 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.916 |

## 7' CLEAR SPAN BY 6' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { FILL } \\ \mathrm{ft} . \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \mathrm{in} . \end{gathered}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \mathrm{SIZE} \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.716 |
| 1 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.716 |
| 2 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.716 |
| 3 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 7 | A | 4 | 5.5 | 4 | 12 | 0.74 |
| 4 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7.5 | 4 | 12 | 0.715 |
| 5 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.738 |
| 6 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.738 |
| 7 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.738 |
| 8 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.787 |
| 9 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.787 |
| 10 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.813 |
| 11 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.813 |
| 12 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.813 |
| 13 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.813 |
| 14 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.813 |
| 15 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.836 |
| 20 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 0.938 |
| 25 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.015 |

## 7' CLEAR SPAN BY 7' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1} \mathrm{BAR}$ |  | $\mathrm{a}_{2}$, h BAR |  | $h_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \hline \text { FILL } \\ & \mathrm{ft} . \\ & \hline \end{aligned}$ | $\begin{gathered} \hline \mathrm{T} \\ \text { in. } \\ \hline \end{gathered}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \\ \hline \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SIZE } \\ \# \\ \hline \end{array}$ | $\begin{array}{\|c} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.807 |
| 1 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.807 |
| 2 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.807 |
| 3 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.807 |
| 4 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.808 |
| 5 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.808 |
| 6 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.808 |
| 7 | 9 | A | 6 | 7 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.808 |
| 8 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 0.86 |
| 9 | 9.5 | A | 6 | 6.5 | 5 | 12 | 5 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 0.86 |
| 10 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 0.913 |
| 11 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 0.913 |
| 12 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 9 | A | 6 | 7 | 5 | 12 | 0.94 |
| 13 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 9 | A | 6 | 7 | 5 | 12 | 0.94 |
| 14 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 9 | A | 6 | 7 | 5 | 12 | 0.94 |
| 15 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 9 | A | 6 | 7 | 5 | 12 | 0.94 |
| 20 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.046 |
| 25 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 11 | A | 6 | 6 | 5 | 12 | 1.156 |

8' CLEAR SPAN BY 2' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { FILL } \\ \mathrm{ft} . \end{gathered}$ | $\begin{aligned} & \mathrm{T} \\ & \mathrm{in} . \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{aligned} & \text { SPC. } \\ & \text { in. } \end{aligned}$ | $\begin{array}{\|c\|} \hline \text { SIZE } \\ \# \end{array}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.657 |
| 1 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.657 |
| 2 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.657 |
| 3 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.657 |
| 4 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.657 |
| 5 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.657 |
| 6 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.657 |
| 7 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.657 |
| 8 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.657 |
| 9 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.685 |
| 10 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.685 |
| 11 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.713 |
| 12 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.713 |
| 13 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.713 |
| 14 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.741 |
| 15 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.741 |
| 20 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.796 |
| 25 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.88 |


| 8' CLEAR SPAN BY 3' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1} \mathrm{BAR}$ |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. <br> Vol. yd. 3 / ft |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{aligned} & \hline \text { W } \\ & \text { in. } \\ & \hline \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.694 |
| 1 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.694 |
| 2 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.694 |
| 3 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.694 |
| 4 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.694 |
| 5 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.694 |
| 6 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.694 |
| 7 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.694 |
| 8 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.694 |
| 9 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.722 |
| 10 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.722 |
| 11 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.75 |
| 12 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.75 |
| 13 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.75 |
| 14 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.778 |
| 15 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.778 |
| 20 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.833 |
| 25 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.917 |

8' CLEAR SPAN BY 4' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft.} . \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{c\|} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.731 |
| 1 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.731 |
| 2 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.731 |
| 3 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.731 |
| 4 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.731 |
| 5 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.731 |
| 6 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.731 |
| 7 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.731 |
| 8 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.731 |
| 9 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.759 |
| 10 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.759 |
| 11 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.787 |
| 12 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.787 |
| 13 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.787 |
| 14 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.815 |
| 15 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.815 |
| 20 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.87 |
| 25 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7.5 | 4 | 12 | 0.993 |


| 8' CLEAR SPAN BY 5' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1} \mathrm{BAR}$ |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. <br> Vol. yd. 3 / ft |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{aligned} & \hline \text { W } \\ & \text { in. } \\ & \hline \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.769 |
| 1 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.769 |
| 2 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.769 |
| 3 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.769 |
| 4 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.769 |
| 5 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.769 |
| 6 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.769 |
| 7 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.769 |
| 8 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 5 | 7.5 | 4 | 12 | 0.769 |
| 9 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7.5 | 4 | 12 | 0.796 |
| 10 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.796 |
| 11 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.824 |
| 12 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.824 |
| 13 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.845 |
| 14 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.873 |
| 15 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.895 |
| 20 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 7 | A | 5 | 6 | 4 | 12 | 0.952 |
| 25 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.082 |

8' CLEAR SPAN BY 6' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { FILL } \\ \mathrm{ft} . \end{gathered}$ | $\begin{aligned} & \mathrm{T} \\ & \mathrm{in} . \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{aligned} & \text { SPC. } \\ & \text { in. } \end{aligned}$ | $\begin{array}{\|c\|} \hline \text { SIZE } \\ \# \end{array}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.806 |
| 1 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.806 |
| 2 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.806 |
| 3 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 7 | A | 4 | 5.5 | 4 | 12 | 0.829 |
| 4 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7.5 | 4 | 12 | 0.829 |
| 5 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.853 |
| 6 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.853 |
| 7 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.853 |
| 8 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.877 |
| 9 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.906 |
| 10 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.906 |
| 11 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.934 |
| 12 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.934 |
| 13 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.934 |
| 14 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.963 |
| 15 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.988 |
| 20 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.07 |
| 25 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.184 |


| 8' CLEAR SPAN BY 7' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v B A R$ |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  |  |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft.} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.897 |
| 1 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.897 |
| 2 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.897 |
| 3 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.897 |
| 4 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.924 |
| 5 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.924 |
| 6 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.924 |
| 7 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.924 |
| 8 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 0.951 |
| 9 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 0.979 |
| 10 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.007 |
| 11 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.036 |
| 12 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.063 |
| 13 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.063 |
| 14 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.093 |
| 15 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.093 |
| 20 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.18 |
| 25 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 11 | A | 6 | 6 | 5 | 12 | 1.326 |

8' CLEAR SPAN BY 8' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1} \mathrm{BAR}$ |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1 |
| 1 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1 |
| 2 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1 |
| 3 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1 |
| 4 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1 |
| 5 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1 |
| 6 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.03 |
| 7 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.03 |
| 8 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.06 |
| 9 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.09 |
| 10 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.09 |
| 11 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.149 |
| 12 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.149 |
| 13 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.149 |
| 14 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.179 |
| 15 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6 | 5 | 12 | 1.21 |
| 20 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 11 | A | 7 | 7 | 6 | 12 | 1.301 |
| 25 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 12 | A | 7 | 7 | 6 | 12 | 1.456 |


| 9' CLEAR SPAN BY 2' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v B A R$ |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  |  |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \hline \text { W } \\ & \text { in. } \\ & \hline \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.753 |
| 1 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.753 |
| 2 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.753 |
| 3 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.722 |
| 4 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.722 |
| 5 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.722 |
| 6 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.722 |
| 7 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.753 |
| 8 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.753 |
| 9 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.815 |
| 10 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.846 |
| 11 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.846 |
| 12 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.846 |
| 13 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.846 |
| 14 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.877 |
| 15 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.877 |
| 20 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.969 |
| 25 | 15 | A | 8 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.031 |

## 9' CLEAR SPAN BY 3' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1} \mathrm{BAR}$ |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { FILL } \\ \mathrm{ft} . \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \mathrm{in} . \end{gathered}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{aligned} & \text { SPC. } \\ & \text { in. } \end{aligned}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.79 |
| 1 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.79 |
| 2 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.79 |
| 3 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.759 |
| 4 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.759 |
| 5 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.759 |
| 6 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.759 |
| 7 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.79 |
| 8 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.79 |
| 9 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.852 |
| 10 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.883 |
| 11 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.883 |
| 12 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.883 |
| 13 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A |  | 5.5 | 4 | 12 | 0.883 |
| 14 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.914 |
| 15 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.914 |
| 20 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.006 |
| 25 | 15 | A | 8 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.068 |


| 9' CLEAR SPAN BY 4' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1} \mathrm{BAR}$ |  | $\mathrm{a}_{2}$, h BAR |  | h, BAR |  | WALL |  | $v B A R$ |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. <br> Vol. yd. ${ }^{3} / \mathrm{ft}$, |
| $\begin{array}{\|c} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{array}$ | $\begin{gathered} \hline \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c} \hline \mathrm{SPC} . \\ \text { in. } \end{array}$ | $\begin{aligned} & \hline \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SPC. } \\ \text { in. } \end{array}$ |  |
| 0 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.827 |
| 1 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.827 |
| 2 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.827 |
| 3 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.796 |
| 4 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.796 |
| 5 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.796 |
| 6 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.796 |
| 7 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.827 |
| 8 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.827 |
| 9 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.889 |
| 10 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.92 |
| 11 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.92 |
| 12 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.92 |
| 13 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.92 |
| 14 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.951 |
| 15 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.951 |
| 20 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 1.043 |
| 25 | 15 | A | 8 | 6 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7.5 | 4 | 12 | 1.146 |

9' CLEAR SPAN BY 5' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft.} . \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{aligned} & \text { SPC. } \\ & \text { in. } \end{aligned}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.864 |
| 1 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.864 |
| 2 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.864 |
| 3 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.833 |
| 4 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.833 |
| 5 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.833 |
| 6 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.833 |
| 7 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.864 |
| 8 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7.5 | 4 | 12 | 0.864 |
| 9 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7.5 | 4 | 12 | 0.926 |
| 10 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.957 |
| 11 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.957 |
| 12 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 0.957 |
| 13 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.979 |
| 14 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.01 |
| 15 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.032 |
| 20 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 6 | 4 | 12 | 1.126 |
| 25 | 15 | A | 8 | 6 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.236 |


| 9' CLEAR SPAN BY 6' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SIZE } \\ \# \end{array}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SIZE } \\ \# \end{array}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SIZE } \\ \# \end{array}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.901 |
| 1 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.901 |
| 2 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.901 |
| 3 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 7 | A | 4 | 5.5 | 4 | 12 | 0.894 |
| 4 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7.5 | 4 | 12 | 0.894 |
| 5 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.918 |
| 6 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.918 |
| 7 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.95 |
| 8 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.974 |
| 9 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.037 |
| 10 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.069 |
| 11 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.069 |
| 12 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.069 |
| 13 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.069 |
| 14 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.1 |
| 15 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.126 |
| 20 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.247 |
| 25 | 15 | A | 8 | 6 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.338 |

9' CLEAR SPAN BY 7' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v B A R$ |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { FILL } \\ \mathrm{ft} . \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{aligned} & \text { SPC. } \\ & \text { in. } \end{aligned}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.993 |
| 1 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.993 |
| 2 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.993 |
| 3 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 7 | A | 5 | 7 | 4 | 12 | 0.961 |
| 4 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.988 |
| 5 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.988 |
| 6 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 5 | 6 | 4 | 12 | 0.988 |
| 7 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.02 |
| 8 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.047 |
| 9 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.111 |
| 10 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.171 |
| 11 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.171 |
| 12 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | $\bigcirc$ | A | 6 | 7 | 5 | 12 | 1.199 |
| 13 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.199 |
| 14 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.231 |
| 15 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.231 |
| 20 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.358 |
| 25 | 15 | A | 8 | 6 | 6 | 12 | 6 | 12 | 11 | A | 6 | 6 | 5 | 12 | 1.482 |


| 9' CLEAR SPAN BY 8' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1} \mathrm{BAR}$ |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. <br> Vol. yd. 3 / ft |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{aligned} & \hline \text { W } \\ & \text { in. } \\ & \hline \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.097 |
| 1 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.097 |
| 2 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.097 |
| 3 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.065 |
| 4 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.065 |
| 5 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.065 |
| 6 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.095 |
| 7 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.127 |
| 8 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.157 |
| 9 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.222 |
| 10 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.255 |
| 11 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.286 |
| 12 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.286 |
| 13 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.286 |
| 14 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.318 |
| 15 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6 | 5 | 12 | 1.35 |
| 20 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 11 | A | 7 | 7 | 6 | 12 | 1.481 |
| 25 | 15 | A | 8 | 6 | 6 | 12 | 6 | 12 | 12 | A | 7 | 7 | 6 | 12 | 1.612 |

Culvert Manual
9' CLEAR SPAN BY 9' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft.} . \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{c\|} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.213 |
| 1 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.213 |
| 2 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.213 |
| 3 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.181 |
| 4 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.181 |
| 5 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.181 |
| 6 | 10 | A | 6 | 6 | 5 | 12 | 5 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.181 |
| 7 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6.5 | 5 | 12 | 1.246 |
| 8 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6.5 | 5 | 12 | 1.246 |
| 9 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6.5 | 5 | 12 | 1.312 |
| 10 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.379 |
| 11 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.379 |
| 12 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.379 |
| 13 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.379 |
| 14 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.446 |
| 15 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.446 |
| 20 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 12 | C | 7 | 7 | 6 | 12 | 1.651 |
| 25 | 15 | A | 8 | 6 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6 | 6 | 12 | 1.719 |


| 10' CLEAR SPAN BY 2' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1} \mathrm{BAR}$ |  | $\mathrm{a}_{2}, \mathrm{~h}$ BAR |  | $\mathrm{h}_{1} \mathrm{BAR}$ |  | WALL |  | $v$ BAR |  | $v_{2}, h_{2}$ BAR |  | $\begin{gathered} \text { Conc. } \\ \text { Vol. } \\ \text { yd. }{ }^{3} / \mathrm{ft} . \end{gathered}$ |
| FILL ft . | $\begin{gathered} \mathrm{T} \\ \mathrm{in} . \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | SPC. in. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | SPC. in. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | SPC. in. |  |
| 0 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 0.889 |
| 1 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 0.889 |
| 2 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 0.889 |
| 3 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 0.855 |
| 4 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 0.855 |
| 5 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 0.855 |
| 6 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 0.855 |
| 7 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 0.889 |
| 8 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 0.923 |
| 9 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 0.923 |
| 10 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 0.923 |
| 11 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 0.957 |
| 12 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 0.991 |
| 13 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 0.991 |
| 14 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 0.991 |
| 15 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.059 |
| 20 | 15 | A | 8 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.127 |
| 25 | 17 | A | 8 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.262 |


| 10' CLEAR SPAN BY 3' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}, \mathrm{~h}$ BAR |  | $h_{1}$ BAR |  | WALL |  | $v B A R$ |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  | $\begin{gathered} \text { Conc. } \\ \text { Vol. } \\ \text { yd. }{ }^{3} / \mathrm{ft} . \end{gathered}$ |
| $\begin{gathered} \text { FILL } \\ \mathrm{ft} . \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{aligned} & \text { SPC. } \\ & \text { in. } \end{aligned}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{aligned} & \mathrm{SPC} . \\ & \text { in. } \end{aligned}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.926 |
| 1 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.926 |
| 2 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.926 |
| 3 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.892 |
| 4 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.892 |
| 5 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.892 |
| 6 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.892 |
| 7 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.926 |
| 8 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.96 |
| 9 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.96 |
| 10 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.96 |
| 11 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.994 |
| 12 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.028 |
| 13 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.028 |
| 14 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.028 |
| 15 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.096 |
| 20 | 15 | A | 8 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.164 |
| 25 | 17 | A | 8 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.299 |


| 10' CLEAR SPAN BY 4' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  | Conc. Vol. yd. $3 / \mathrm{ft}$. |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \end{gathered}$ | $\begin{gathered} \hline \mathrm{T} \\ \mathrm{in} . \end{gathered}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.963 |
| 1 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.963 |
| 2 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.963 |
| 3 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.929 |
| 4 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.929 |
| 5 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.929 |
| 6 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.929 |
| 7 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.963 |
| 8 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.997 |
| 9 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.997 |
| 10 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.997 |
| 11 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.031 |
| 12 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.065 |
| 13 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.065 |
| 14 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.065 |
| 15 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.133 |
| 20 | 15 | A | 8 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 1.201 |
| 25 | 17 | A | 8 | 5.5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7.5 | 4 | 12 | 1.379 |

Culvert Manual
Section 3 - Design

| 10' CLEAR SPAN BY 5' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | W <br> in. | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1 |
| 1 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1 |
| 2 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1 |
| 3 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.966 |
| 4 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.966 |
| 5 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.966 |
| 6 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 0.966 |
| 7 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1 |
| 8 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7.5 | 4 | 12 | 1.034 |
| 9 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7.5 | 4 | 12 | 1.034 |
| 10 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 1.034 |
| 11 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 1.068 |
| 12 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 1.102 |
| 13 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.124 |
| 14 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.124 |
| 15 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.216 |
| 20 | 15 | A | 8 | 6.5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 6 | 4 | 12 | 1.284 |
| 25 | 17 | A | 8 | 5.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.471 |


| 10' CLEAR SPAN BY 6' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \end{gathered}$ | $\begin{gathered} \hline \mathrm{T} \\ \mathrm{in} . \end{gathered}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.037 |
| 1 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.037 |
| 2 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.037 |
| 3 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 7 | A | 4 | 5.5 | 4 | 12 | 1.028 |
| 4 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7.5 | 4 | 12 | 1.028 |
| 5 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.052 |
| 6 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.052 |
| 7 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.086 |
| 8 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.146 |
| 9 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.146 |
| 10 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.146 |
| 11 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.181 |
| 12 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.215 |
| 13 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.215 |
| 14 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.215 |
| 15 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.311 |
| 20 | 15 | A | 8 | 6.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.407 |
| 25 | 17 | A | 8 | 5.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.576 |


| 10' CLEAR SPAN BY 7' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1} \mathrm{BAR}$ |  | $\mathrm{a}_{2}$, h BAR |  | $h_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3}$ /ft. |
| $\begin{array}{\|l} \hline \text { FILL } \\ \mathrm{ft} . \end{array}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.13 |
| 1 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.13 |
| 2 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.13 |
| 3 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.095 |
| 4 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.123 |
| 5 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.123 |
| 6 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.123 |
| 7 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.157 |
| 8 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.22 |
| 9 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.22 |
| 10 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.248 |
| 11 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.283 |
| 12 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.347 |
| 13 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.347 |
| 14 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.347 |
| 15 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.418 |
| 20 | 15 | A | 8 | 6.5 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.519 |
| 25 | 17 | A | 8 | 5.5 | 6 | 12 | 6 | 12 | 11 | A | 6 | 6 | 5 | 12 | 1.723 |


| 10' CLEAR SPAN BY 8' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1} \mathrm{BAR}$ |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \end{gathered}$ | $\begin{gathered} \hline \mathrm{T} \\ \mathrm{in} . \end{gathered}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.235 |
| 1 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.235 |
| 2 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.235 |
| 3 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.2 |
| 4 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.2 |
| 5 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.2 |
| 6 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.23 |
| 7 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.265 |
| 8 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.332 |
| 9 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.332 |
| 10 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.332 |
| 11 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.399 |
| 12 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.434 |
| 13 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.434 |
| 14 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.434 |
| 15 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6 | 5 | 12 | 1.538 |
| 20 | 15 | A | 8 | 6.5 | 6 | 12 | 6 | 12 | 11 | A | 7 | 7 | 6 | 12 | 1.643 |
| 25 | 17 | A | 8 | 5.5 | 6 | 12 | 6 | 12 | 12 | A | 7 | 7 | 6 | 12 | 1.855 |

Culvert Manual
Section 3 - Design

| 10' CLEAR SPAN BY 9' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  |  |
| $\begin{gathered} \text { FILL } \\ \mathrm{ft.} . \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \mathrm{SIZE} \\ \# \end{gathered}$ | $\begin{aligned} & \text { SPC. } \\ & \text { in. } \end{aligned}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.352 |
| 1 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.352 |
| 2 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.352 |
| 3 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.316 |
| 4 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.316 |
| 5 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.316 |
| 6 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.316 |
| 7 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6.5 | 5 | 12 | 1.386 |
| 8 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6.5 | 5 | 12 | 1.422 |
| 9 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6.5 | 5 | 12 | 1.422 |
| 10 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.456 |
| 11 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.492 |
| 12 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.528 |
| 13 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.528 |
| 14 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.563 |
| 15 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.635 |
| 20 | 15 | A | 8 | 6.5 | 6 | 12 | 6 | 12 | 12 | C | 7 | 7 | 6 | 12 | 1.815 |
| 25 | 17 | A | 8 | 5.5 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6 | 6 | 12 | 1.963 |


| 10' CLEAR SPAN BY 10' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  |  |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \hline \text { W } \\ & \text { in. } \\ & \hline \end{aligned}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SIZE } \\ \# \\ \hline \end{array}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.481 |
| 1 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.481 |
| 2 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.481 |
| 3 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.445 |
| 4 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.445 |
| 5 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.445 |
| 6 | 11 | A | 7 | 7 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.445 |
| 7 | 12 | A | 7 | 7 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.481 |
| 8 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.517 |
| 9 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 11 | B | 6 | 6 | 5 | 12 | 1.555 |
| 10 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.555 |
| 11 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.629 |
| 12 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.665 |
| 13 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.665 |
| 14 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 12 | B | 7 | 7 | 6 | 12 | 1.703 |
| 15 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 1.815 |
| 20 | 15 | A | 8 | 6.5 | 6 | 12 | 6 | 12 | 13 | C | 7 | 6 | 6 | 12 | 1.928 |
| 25 | 17 | A | 8 | 5.5 | 6 | 12 | 6 | 12 | 14 | C | 7 | 5.5 | 6 | 12 | 2.157 |

11'CLEAR SPAN BY 2' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. $3 / \mathrm{ft}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { FILL } \\ \mathrm{ft.} \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1 |
| 1 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1 |
| 2 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1 |
| 3 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1 |
| 4 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1 |
| 5 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1 |
| 6 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1 |
| 7 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1 |
| 8 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.037 |
| 9 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.074 |
| 10 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.111 |
| 11 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.111 |
| 12 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.111 |
| 13 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.111 |
| 14 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.148 |
| 15 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.185 |
| 20 | 17 | A | 8 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.37 |
| 25 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.444 |


| 11' CLEAR SPAN BY 3' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  |  |
| $\begin{array}{\|c\|} \hline \text { FILL } \\ \mathrm{ft} . \end{array}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.037 |
| 1 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.037 |
| 2 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.037 |
| 3 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.037 |
| 4 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.037 |
| 5 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.037 |
| 6 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.037 |
| 7 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.037 |
| 8 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.074 |
| 9 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.111 |
| 10 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.148 |
| 11 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.148 |
| 12 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.148 |
| 13 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.148 |
| 14 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.185 |
| 15 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.222 |
| 20 | 17 | A | 8 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.407 |
| 25 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.481 |

11' CLEAR SPAN BY 4' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1} \mathrm{BAR}$ |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  | Conc. <br> Vol. <br> yd. $3 / \mathrm{ft}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|c} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{array}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | SIZE | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | SIZE | $\begin{aligned} & \text { SPC. } \\ & \text { in. } \end{aligned}$ | SIZE | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | SIZE | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | SIZE | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.074 |
| 1 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.074 |
| 2 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.074 |
| 3 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.074 |
| 4 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.074 |
| 5 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.074 |
| 6 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.074 |
| 7 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.074 |
| 8 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.111 |
| 9 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.148 |
| 10 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.185 |
| 11 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.185 |
| 12 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.185 |
| 13 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.185 |
| 14 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.222 |
| 15 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.259 |
| 20 | 17 | A | 8 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 1.444 |
| 25 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7.5 | 4 | 12 | 1.562 |


| 11' CLEAR SPAN BY 5' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{T} \\ \mathrm{in} . \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.111 |
| 1 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.111 |
| 2 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.111 |
| 3 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.111 |
| 4 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.111 |
| 5 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.111 |
| 6 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.111 |
| 7 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.111 |
| 8 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7.5 | 4 | 12 | 1.148 |
| 9 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7.5 | 4 | 12 | 1.185 |
| 10 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 1.222 |
| 11 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 1.222 |
| 12 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 1.222 |
| 13 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.245 |
| 14 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.282 |
| 15 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.343 |
| 20 | 17 | A | 8 | 5.5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 6 | 4 | 12 | 1.53 |
| 25 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.655 |

11'CLEAR SPAN BY 6' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. 3 / ft. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { FILL } \\ \mathrm{ft.} \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.148 |
| 1 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.148 |
| 2 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.148 |
| 3 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 7 | A | 4 | 5.5 | 4 | 12 | 1.173 |
| 4 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7.5 | 4 | 12 | 1.173 |
| 5 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.198 |
| 6 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.198 |
| 7 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.198 |
| 8 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.261 |
| 9 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.299 |
| 10 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.336 |
| 11 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.336 |
| 12 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.336 |
| 13 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.336 |
| 14 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.374 |
| 15 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.438 |
| 20 | 17 | A | 8 | 5.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.656 |
| 25 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.761 |


| 11' CLEAR SPAN BY 7' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{T} \\ \mathrm{in} . \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.241 |
| 1 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.241 |
| 2 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.241 |
| 3 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.241 |
| 4 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.269 |
| 5 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.269 |
| 6 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.269 |
| 7 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.269 |
| 8 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.335 |
| 9 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.373 |
| 10 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.44 |
| 11 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.44 |
| 12 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.469 |
| 13 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.469 |
| 14 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.508 |
| 15 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.546 |
| 20 | 17 | A | 8 | 5.5 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.77 |
| 25 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 11 | A | 6 | 6 | 5 | 12 | 1.91 |

Culvert Manual
Section 3 - Design
11' CLEAR SPAN BY 8' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1} \mathrm{BAR}$ |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v B A R$ |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SIZE } \\ \# \end{array}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.347 |
| 1 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.347 |
| 2 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.347 |
| 3 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.347 |
| 4 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.347 |
| 5 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.347 |
| 6 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.378 |
| 7 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.378 |
| 8 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.448 |
| 9 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.486 |
| 10 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.525 |
| 11 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.557 |
| 12 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.557 |
| 13 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.557 |
| 14 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.595 |
| 15 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6 | 5 | 12 | 1.667 |
| 20 | 17 | A | 8 | 5.5 | 6 | 12 | 6 | 12 | 11 | A | 7 | 7 | 6 | 12 | 1.896 |
| 25 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 12 | A | 7 | 7 | 6 | 12 | 2.043 |


| 11' CLEAR SPAN BY 9' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v B A R$ |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. 3 / ft. |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft.} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{T} \\ \text { in. } \\ \hline \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{array}$ | W | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.465 |
| 1 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.465 |
| 2 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.465 |
| 3 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.465 |
| 4 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.465 |
| 5 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.465 |
| 6 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.465 |
| 7 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6.5 | 5 | 12 | 1.499 |
| 8 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6.5 | 5 | 12 | 1.538 |
| 9 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6.5 | 5 | 12 | 1.576 |
| 10 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.65 |
| 11 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.65 |
| 12 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.65 |
| 13 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.65 |
| 14 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.725 |
| 15 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.764 |
| 20 | 17 | A | 8 | 5.5 | 6 | 12 | 6 | 12 | 12 | C | 7 | 7 | 6 | 12 | 2.071 |
| 25 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6 | 6 | 12 | 2.151 |

11' CLEAR SPAN BY 10' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1} \mathrm{BAR}$ |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.595 |
| 1 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.595 |
| 2 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.595 |
| 3 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.595 |
| 4 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.595 |
| 5 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.595 |
| 6 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.595 |
| 7 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.595 |
| 8 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.634 |
| 9 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 11 | B | 6 | 6 | 5 | 12 | 1.711 |
| 10 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.75 |
| 11 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.788 |
| 12 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.788 |
| 13 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.788 |
| 14 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 12 | B | 7 | 7 | 6 | 12 | 1.866 |
| 15 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 1.944 |
| 20 | 17 | A | 8 | 5.5 | 6 | 12 | 6 | 12 | 13 | C | 7 | 6 | 6 | 12 | 2.185 |
| 25 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 14 | C | 7 | 5.5 | 6 | 12 | 2.346 |


| 11' CLEAR SPAN BY 11' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1} \mathrm{BAR}$ |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v B A R$ |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. <br> Vol. yd. 3 / ft |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{aligned} & \hline \text { W } \\ & \text { in. } \\ & \hline \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.737 |
| 1 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.737 |
| 2 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.737 |
| 3 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.737 |
| 4 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.737 |
| 5 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.737 |
| 6 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.737 |
| 7 | 12 | A | 7 | 6.5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.737 |
| 8 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.777 |
| 9 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 12 | B | 7 | 7 | 6 | 12 | 1.857 |
| 10 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 1.938 |
| 11 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 1.938 |
| 12 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 1.938 |
| 13 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 1.938 |
| 14 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 13 | C | 7 | 6.5 | 6 | 12 | 2.02 |
| 15 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 13 | C | 7 | 6 | 6 | 12 | 2.06 |
| 20 | 17 | A | 8 | 5.5 | 6 | 12 | 6 | 12 | 14 | C | 7 | 5.5 | 6 | 12 | 2.391 |
| 25 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 15 | C | 7 | 5 | 6 | 12 | 2.517 |

Culvert Manual
Section 3 - Design

| 12' CLEAR SPAN BY 2' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft.} . \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{aligned} & \text { SPC. } \\ & \text { in. } \end{aligned}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{aligned} & \text { SPC. } \\ & \text { in. } \end{aligned}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | W in. | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.117 |
| 1 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.117 |
| 2 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.117 |
| 3 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.117 |
| 4 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.117 |
| 5 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.117 |
| 6 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.117 |
| 7 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.117 |
| 8 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.198 |
| 9 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.198 |
| 10 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.278 |
| 11 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.278 |
| 12 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.278 |
| 13 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.278 |
| 14 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.358 |
| 15 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.358 |
| 20 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.559 |
| 25 | 20 | A | 9 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | A | 12 | 1.719 |


| 12' CLEAR SPAN BY 3' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \end{gathered}$ | $\begin{gathered} \hline \mathrm{T} \\ \mathrm{in} . \end{gathered}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.154 |
| 1 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.154 |
| 2 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.154 |
| 3 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.154 |
| 4 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.154 |
| 5 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.154 |
| 6 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.154 |
| 7 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.154 |
| 8 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.235 |
| 9 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.235 |
| 10 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.315 |
| 11 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.315 |
| 12 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.315 |
| 13 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.315 |
| 14 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.395 |
| 15 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.395 |
| 20 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.596 |
| 25 | 20 | A | 9 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.756 |


| 12' CLEAR SPAN BY 4' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | $\begin{array}{\|c\|} \hline \text { Conc. } \\ \text { Vol. } \\ \text { yd. } 3 / \mathrm{ft} . \end{array}$ |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{aligned} & \text { SPC. } \\ & \text { in. } \end{aligned}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.191 |
| 1 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.191 |
| 2 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.191 |
| 3 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.191 |
| 4 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.191 |
| 5 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.191 |
| 6 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.191 |
| 7 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.191 |
| 8 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.272 |
| 9 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.272 |
| 10 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.352 |
| 11 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.352 |
| 12 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.352 |
| 13 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.352 |
| 14 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.432 |
| 15 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.432 |
| 20 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 1.633 |
| 25 | 20 | A | 9 | 6 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7.5 | 4 | 12 | 1.839 |


| 12' CLEAR SPAN BY 5' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  | Conc. Vol. yd. $3 / \mathrm{ft}$. |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \end{gathered}$ | $\begin{gathered} \hline \mathrm{T} \\ \mathrm{in} . \end{gathered}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.228 |
| 1 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.228 |
| 2 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.228 |
| 3 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.228 |
| 4 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.228 |
| 5 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.228 |
| 6 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.228 |
| 7 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.228 |
| 8 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7.5 | 4 | 12 | 1.309 |
| 9 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7.5 | 4 | 12 | 1.309 |
| 10 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 1.389 |
| 11 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 1.389 |
| 12 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 6 | A | 5 | 7 | 4 | 12 | 1.389 |
| 13 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.412 |
| 14 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.493 |
| 15 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.516 |
| 20 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 7 | A | 5 | 6 | 4 | 12 | 1.72 |
| 25 | 20 | A | 9 | 6 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.934 |

Culvert Manual
Section 3 - Design

| 12' CLEAR SPAN BY 6' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft.} . \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{aligned} & \text { SPC. } \\ & \text { in. } \end{aligned}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{aligned} & \text { SPC. } \\ & \text { in. } \end{aligned}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | W in. | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{c\|} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.265 |
| 1 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.265 |
| 2 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 6 | A | 4 | 5.5 | 4 | 12 | 1.265 |
| 3 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 7 | A | 4 | 5.5 | 4 | 12 | 1.291 |
| 4 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7.5 | 4 | 12 | 1.291 |
| 5 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.316 |
| 6 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.316 |
| 7 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.316 |
| 8 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.423 |
| 9 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.423 |
| 10 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.505 |
| 11 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.505 |
| 12 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.505 |
| 13 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.505 |
| 14 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.586 |
| 15 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.613 |
| 20 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.847 |
| 25 | 20 | A | 9 | 6 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 2.042 |


| 12' CLEAR SPAN BY 7' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \end{gathered}$ | $\begin{gathered} \hline \mathrm{T} \\ \mathrm{in} . \end{gathered}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.359 |
| 1 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.359 |
| 2 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.359 |
| 3 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 7 | A | 5 | 7 | 4 | 12 | 1.359 |
| 4 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.387 |
| 5 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.387 |
| 6 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.387 |
| 7 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 5 | 6 | 4 | 12 | 1.387 |
| 8 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.498 |
| 9 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.498 |
| 10 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.61 |
| 11 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.61 |
| 12 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.639 |
| 13 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.639 |
| 14 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.722 |
| 15 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.722 |
| 20 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.962 |
| 25 | 20 | A | 9 | 6 | 6 | 12 | 6 | 12 | 11 | A | 6 | 6 | 5 | 12 | 2.194 |


| 12' CLEAR SPAN BY 8' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft.} . \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{aligned} & \text { SPC. } \\ & \text { in. } \end{aligned}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{aligned} & \text { SPC. } \\ & \text { in. } \end{aligned}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | W in. | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.465 |
| 1 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.465 |
| 2 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.465 |
| 3 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.465 |
| 4 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.465 |
| 5 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 8 | A | 6 | 7.5 | 5 | 12 | 1.465 |
| 6 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.496 |
| 7 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7.5 | 5 | 12 | 1.496 |
| 8 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.611 |
| 9 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.611 |
| 10 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 9 | A | 6 | 7 | 5 | 12 | 1.694 |
| 11 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.727 |
| 12 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.727 |
| 13 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.727 |
| 14 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6.5 | 5 | 12 | 1.811 |
| 15 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 10 | A | 6 | 6 | 5 | 12 | 1.844 |
| 20 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 11 | A | 7 | 7 | 6 | 12 | 2.089 |
| 25 | 20 | A | 9 | 6 | 6 | 12 | 6 | 12 | 12 | A | 7 | 7 | 6 | 12 | 2.329 |


| 12' CLEAR SPAN BY 9' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  | Conc. Vol. yd. ${ }^{3} / \mathrm{ft}$. |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \end{gathered}$ | $\begin{gathered} \hline \mathrm{T} \\ \mathrm{in} . \end{gathered}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \hline \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.583 |
| 1 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.583 |
| 2 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.583 |
| 3 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.583 |
| 4 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.583 |
| 5 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.583 |
| 6 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 9 | B | 6 | 7 | 5 | 12 | 1.583 |
| 7 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6.5 | 5 | 12 | 1.618 |
| 8 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6.5 | 5 | 12 | 1.702 |
| 9 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6.5 | 5 | 12 | 1.702 |
| 10 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.821 |
| 11 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.821 |
| 12 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.821 |
| 13 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.821 |
| 14 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.941 |
| 15 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.941 |
| 20 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 12 | C | 7 | 7 | 6 | 12 | 2.265 |
| 25 | 20 | A | 9 | 6 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6 | 6 | 12 | 2.438 |

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12' CLEAR SPAN BY 10' CLEAR HEIGHT

| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. $3 / \mathrm{ft}$. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{\|c\|} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{array}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{aligned} & \text { SPC. } \\ & \text { in. } \end{aligned}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{aligned} & \text { SPC. } \\ & \text { in. } \end{aligned}$ | $\begin{aligned} & \text { W } \\ & \text { in. } \end{aligned}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ |  |
| 0 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.714 |
| 1 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.714 |
| 2 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.714 |
| 3 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.714 |
| 4 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.714 |
| 5 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.714 |
| 6 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.714 |
| 7 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.714 |
| 8 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 10 | B | 6 | 6 | 5 | 12 | 1.798 |
| 9 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 11 | B | 6 | 6 | 5 | 12 | 1.836 |
| 10 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.921 |
| 11 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.96 |
| 12 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.96 |
| 13 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.96 |
| 14 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 12 | B | 7 | 7 | 6 | 12 | 2.084 |
| 15 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 2.123 |
| 20 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 13 | C | 7 | 6 | 6 | 12 | 2.38 |
| 25 | 20 | A | 9 | 6 | 6 | 12 | 6 | 12 | 14 | C | 7 | 5.5 | 6 | 12 | 2.637 |


| 12' CLEAR SPAN BY 11' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2} \mathrm{BAR}$ |  |  |
| $\begin{array}{\|c\|} \hline \text { FILL } \\ \mathrm{ft} . \end{array}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{array}{\|l\|} \hline \mathrm{W} \\ \mathrm{in} . \\ \hline \end{array}$ | SEC. | $\begin{gathered} \hline \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.857 |
| 1 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.857 |
| 2 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.857 |
| 3 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.857 |
| 4 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.857 |
| 5 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.857 |
| 6 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.857 |
| 7 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.857 |
| 8 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 11 | B | 7 | 7 | 6 | 12 | 1.942 |
| 9 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 12 | B | 7 | 7 | 6 | 12 | 1.984 |
| 10 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 2.111 |
| 11 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 2.111 |
| 12 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 2.111 |
| 13 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 2.111 |
| 14 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 13 | C | 7 | 6.5 | 6 | 12 | 2.24 |
| 15 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 13 | C | 7 | 6 | 6 | 12 | 2.24 |
| 20 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 14 | C | 7 | 5.5 | 6 | 12 | 2.587 |
| 25 | 20 | A | 9 | 6 | 6 | 12 | 6 | 12 | 15 | C | 7 | 5 | 6 | 12 | 2.809 |


| 12' CLEAR SPAN BY 12' CLEAR HEIGHT |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TOP SLAB |  |  | $\mathrm{a}_{1}$ BAR |  | $\mathrm{a}_{2}$, h BAR |  | $\mathrm{h}_{1}$ BAR |  | WALL |  | $v$ BAR |  | $\mathrm{v}_{2}, \mathrm{~h}_{2}$ BAR |  | Conc. Vol. yd. ${ }^{3} / \mathrm{f}$ |
| $\begin{gathered} \hline \text { FILL } \\ \mathrm{ft} . \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{T} \\ \text { in. } \end{gathered}$ | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{array}{\|c} \hline \text { SPC. } \\ \text { in. } \end{array}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | W <br> in. | SEC. | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \text { SPC. } \\ \text { in. } \end{gathered}$ | $\begin{gathered} \text { SIZE } \\ \# \end{gathered}$ | $\begin{gathered} \mathrm{SPC} . \\ \text { in. } \end{gathered}$ |  |
| 0 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 2.012 |
| 1 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 2.012 |
| 2 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 2.012 |
| 3 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 2.012 |
| 4 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 2.012 |
| 5 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 2.012 |
| 6 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 2.012 |
| 7 | 13 | A | 7 | 6 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 2.012 |
| 8 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 2.099 |
| 9 | 14 | A | 7 | 5.5 | 6 | 12 | 6 | 12 | 12 | C | 7 | 6.5 | 6 | 12 | 2.099 |
| 10 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 13 | C | 7 | 6 | 6 | 12 | 2.23 |
| 11 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 13 | C | 7 | 6 | 6 | 12 | 2.23 |
| 12 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 13 | C | 7 | 6 | 6 | 12 | 2.23 |
| 13 | 15 | A | 7 | 5 | 6 | 12 | 6 | 12 | 13 | C | 7 | 5.5 | 6 | 12 | 2.23 |
| 14 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 13 | C | 7 | 5.5 | 6 | 12 | 2.362 |
| 15 | 16 | A | 8 | 6 | 6 | 12 | 6 | 12 | 14 | C | 7 | 5.5 | 6 | 12 | 2.407 |
| 20 | 18 | A | 9 | 6.5 | 6 | 12 | 6 | 12 | 15 | C | 7 | 5 | 6 | 12 | 2.767 |
| 25 | 20 | A | 9 | 6 | 6 | 12 | 6 | 12 | 16 | C | 8 | 6 | 6 | 12 | 3.041 |

## Section 4 Headwalls and Wingwalls

### 4.1 General

The focus of this section is end treatments for cast-in-place concrete box culverts. Standard end sections for precast concrete box culverts are available on base sheets and are not discussed in this section.

Except as noted, all loads, load combinations, and load modifiers were calculated in accordance with Section 3 of the Culvert Manual.

### 4.1.1 Loads

### 4.1.1.1 Live Loads

Live load was included in the development of the design charts and tables in this section. The charts and tables are not applicable for wingwalls built parallel to the roadway with traffic lanes within a distance of one-half the wall design height. If this case occurs, a separate design is required, using live load surcharge pressure according to Article 3.11.6.4 of the AASHTO LRFD Bridge Design Specifications.

The wingwalls in this section are not designed to withstand vehicular impact loading. If a railing or parapet is required to be placed on a wingwall, a separate design is required and the standard designs in this chapter shall not be used.

### 4.1.1.2 Lateral Earth Pressure Loads

For horizontal cantilever and two-way cantilever L-type walls, the walls were designed assuming active pressures, and checked using at-rest earth pressures. For T-type walls, and permanent steel sheet piling walls, active earth pressure was assumed.

Table 3.11.5.5-1 of the AASHTO LRFD Bridge Design Specifications gives values of at-rest and active earth pressures for various types of soil, assuming either zero (flat) backslope or 25 degree backslope. The values in AASHTO are based on an angle of internal friction of 30
degrees. To accommodate a smaller angle of internal friction ( 28 degrees), and a larger backslope variation (from zero to 26.56 degrees, which corresponds to a $1: 2(\mathrm{~V}: \mathrm{H})$ backslope), values from Table 3.11.5.5-1 of the AASHTO LRFD Bridge Design Specifications were interpolated and extrapolated to create the following Table 4.1.1.2-1. This figure shows earth pressures in the horizontal and vertical directions for both the active and at-rest state for all applicable backslope angles. The backslope angle shall be measured perpendicular to the face of the wall, and calculated using the procedure shown in Figure 4.1.1.2-2.

|  | HORIZONTAL CANTILEVER or |  | SHEET PILING or |  |
| :---: | :---: | :---: | :---: | :---: |
|  | TWO-WAY CANTILEVER L-TYPE | VERTICAL CANTILEVER T-TYPE |  |  |
| ANGLE OF <br> BACKFILL | $P_{H}(\mathrm{psf})$ | $\mathrm{P}_{\mathrm{V}}(\mathrm{psf})$ | $\mathrm{P}_{\mathrm{H}}(\mathrm{psf})$ | $\mathrm{P}_{\mathrm{V}}(\mathrm{psf})$ |
| 0 | 60 | 0 | 43 | 0 |
| 2 | 60 | 2 | 43 | 2 |
| 4 | 61 | 4 | 44 | 3 |
| 6 | 62 | 7 | 44 | 5 |
| 8 | 63 | 9 | 44 | 6 |
| 10 | 63 | 11 | 45 | 8 |
| 12 | 64 | 14 | 46 | 10 |
| 14 | 64 | 16 | 47 | 12 |
| 16 | 65 | 19 | 48 | 14 |
| 18 | 65 | 21 | 50 | 16 |
| 20 | 66 | 24 | 52 | 19 |
| 22 | 67 | 27 | 55 | 22 |
| 24 | 68 | 30 | 59 | 26 |
| 26 | 70 | 34 | 66 | 32 |
| 26.56 | 71 | 35 | 70 | 35 |

Table 4.1.1.2-1


Figure 4.1.1.2-2
4.1.2 Types of Wingwalls and Applications

For most cast-in-place concrete box culverts, horizontal cantilever wingwalls are the most economical and preferred wall type.

Horizontal cantilever wingwalls are limited to 16 feet in length. If longer walls are required, twoway L-type cantilever wingwalls may be used for lengths of up to 30 feet. For longer walls, another alternative is to use a horizontal cantilever wall for the first 16 feet, then the remainder of the length may be made up using a different type of wall such as permanent steel sheet piling or soldier pile.

For culverts with large skews and/or high rises, cast-in-place concrete walls may become very large and cost-prohibitive. In these cases, sheet pile wingwalls or soldier pile wingwalls may become an economical alternative.

Weak soils or high rock elevations may preclude the use of certain types of walls. The design engineer should verify that the wall type used is consistent with the soil conditions prior to design.

### 4.1.3 Wingwall Geometry

### 4.1.3.1 Wingwall Length

The length of the wingwall shall be determined from the chart shown in Figure 4.1.3.1-2 using the parameters shown in Figure 4.1.3.1-1. The wingwall length shall be rounded to the nearest three inches.


Figure 4.1.3.1-1


$$
\begin{aligned}
& \text { WINGWALL LENGTH CHART } \\
& \text { HORIZONTAL AND VERTICAL } \\
& \text { CANTILEVER 1:2 (V:H) SLOPE }
\end{aligned}
$$

Figure 4.1.3.1-2

### 4.1.3.2 Wingwall and Footing Thicknesses

The minimum wall thickness of the horizontal cantilever wingwalls is eight inches, and increases in increments of one inch.

The minimum wall and footing thickesses for two-way L-type cantilever wingwalls is six inches and increases in increments of one inch.

The minimum stem thickness of the T-type vertical cantilever wingwall is 10 inches and increases in increments of one inch up to 12 inches.

For two-way cantilever L-type and vertical cantilever T-type, no batter is provided when the stem thickness is equal to or less than 12 inches. The maximum thickness at the top of the stem is 12 inches. For stems requiring thickness greater than 12 inches at the base, the stem base thickness is increased in increments of one inch and batter is provided to the back face (the face in contact with the earth), while maintaining constant vertical slope.

The minimum spread footing thickness of the T-type cantilever wingwall is dependent upon the required development length for epoxy-coated hooked reinforcement, of the size required for strength.

### 4.1.3.3 Wingwall Design Heights

The horizontal cantilever wingwall design height is taken as the difference between the highest top of wingwall elevation and the invert elevation.

The two-way L-type cantilever wingwall design height is taken as the difference between six inches below the top of wall elevation and the top of footing elevation.

The vertical cantilever T-type design height is taken as the difference between six inches below the highest wall elevation and the bottom of footing elevation.

Sample calculations for design height for each of these types of walls are shown in Sections 4.2.3, 4.3.3, and 4.4.3, respectively.

### 4.1.4 Reinforcement Design and Details

The size and spacing of all main reinforcement for wingwalls is given in the tables, with the exception of the horizontal cantilever wingwall reinforcement, which is given in a chart. Unless otherwise shown in the table, all reinforcement lengths shall be given on the drawings to the nearest inch. The minimum bar lap length shall be as specified in Section 5 and based on the larger bar size.

Vertical reinforcement in wall stems for walls with differing heights shall utilize field cutting diagrams.

When possible, the maximum reinforcement ratio ( $\rho$ ) used in the design of the wingwalls is limited to approximately $0.375 \rho_{\mathrm{b}}$, where $\rho_{\mathrm{b}}$ is the balanced reinforcement ratio. For some vertical cantilever walls, this limitation was raised to $0.6 \rho_{\mathrm{b}}$ to avoid excessively thick walls.

### 4.1.5 Headwalls

The width of the headwall shall be 12 inches for all culverts with skews up to and including 30 degrees, and 18 inches for all culverts with skews greater than 30 degrees. Standard headwall designs are given in Figure 4.1.5-1. Size \#4 stirrup reinforcement shall be provided at 12 inch centers when the span length (taken along the skew) is less than or equal to 20 feet. Size \#5 stirrup reinforcement shall be provided at 12 inch centers when the span length (taken along the skew) is 20 feet in length or greater.

For design assumptions, the headwall is assumed to act as an edge beam. For culverts with fills less than two feet, the headwall is reinforced to support additional moment due to live load according to Article 4.6.2.10 of the AASHTO LRFD Bridge Design Specifications. For fills two feet or more, the headwall is reinforced to support a live load distributed through the fill according to Article 3.6.1.2.6 of the AASHTO LRFD Bridge Design Specifications. For skewed culverts, the edge beam is reinforced to support the half of the slab, including the portion of fill above the slab, that is unsupported as a result of the skew.

The headwall corner dimensions shown as $X, X_{1}$, and $X_{2}$ shown in Figure 4.1.5-2 are listed in tables shown in Figures 4.1.5-3 and 4.1.5-4. Figure 4.1.5-5 shows an example for calculating headwall corner dimensions.

Headwall drain details are given in the Culvert Details cell library. These drains consist of a three inch PVC drain cast into the concrete vertically through the top slab, six inches from the inside face of the headwall. The top of the drain is covered with an aggregate block that is placed on geotechnical fabric. Headwall drains shall be placed at midspan at each end of each cell of cast-in-place culverts and cast-in-place end sections.

### 4.1.6 Connection Collar Details for Culvert Extensions

Details for connection collars for box culvert extensions are given in the Culvert Details cell library. Two details are given. In the first, the collar is monolithic with the culvert extension. This may be used for cast-in-place culvert extensions. In the second, the culvert is not monolithic with the extension, which may be used for either precast or cast-in-place sections.


Figure 4.1.5-1


Figure 4.1.5-2


Figure 4.1.5-3

| $$ | $\begin{aligned} & \frac{3}{\text { D }} \\ & \stackrel{\rightharpoonup}{U} \end{aligned}$ |  | $\bigcirc$ | i | $\stackrel{\circ}{\mathrm{O}}$ | $\underset{\sim}{\circ}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{0} \end{aligned}$ | $\stackrel{\circ}{\stackrel{i}{N}}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{n} \end{aligned}$ | $\stackrel{\circ}{\stackrel{i}{n}}$ | $\stackrel{\circ}{\circ}$ | $\begin{aligned} & \circ \\ & \stackrel{i}{7} \end{aligned}$ | $\begin{aligned} & \circ \\ & 0 \\ & \text { م } \end{aligned}$ | $\begin{aligned} & 0 \\ & \stackrel{i}{n} \end{aligned}$ | $\begin{aligned} & \circ \\ & 0 \\ & 6 \end{aligned}$ | $\circ$ $i$ 6 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ${ }_{*}^{*}$ | $\begin{aligned} & \overline{0} \\ & \vdots \\ & \vdots \end{aligned}$ | $\begin{aligned} & = \\ & i \\ & 0 \\ & \vdots \\ & i \end{aligned}$ | $\begin{aligned} & e_{\infty} \\ & 0 \\ & \vdots \\ & \vdots \end{aligned}$ | $\begin{aligned} & = \\ & m^{\infty} \\ & \vdots \\ & i \end{aligned}$ | $\begin{aligned} & =\infty \\ & \wedge^{\infty} \\ & \vdots \\ & \vdots \end{aligned}$ | $\begin{aligned} & = \\ & \underset{\sim}{\sim} \\ & \vdots \end{aligned}$ | $\begin{aligned} & = \\ & m^{\sigma} \\ & \underset{\sim}{1} \\ & \stackrel{1}{2} \end{aligned}$ | $\begin{aligned} & = \\ & \frac{\pi}{m} \\ & \stackrel{1}{-} \end{aligned}$ | $\begin{aligned} & = \\ & m^{*} \\ & M \\ & \vdots \end{aligned}$ | $\begin{aligned} & =\sigma \\ & \dot{\sigma} \\ & i \end{aligned}$ | $\begin{aligned} & = \\ & i^{\infty} \\ & + \\ & \vdots \\ & \vdots \end{aligned}$ | $\begin{aligned} & = \\ & \stackrel{\pi}{n} \\ & \vdots \end{aligned}$ | $\begin{aligned} & =\infty \\ & 0^{\infty} \\ & \sim \\ & 1 \\ & \vdots \end{aligned}$ | $\begin{aligned} & = \\ & i \\ & \vdots \\ & \vdots \end{aligned}$ |  |
|  |  | $\bar{x}^{-1}$ | $\begin{aligned} & \bar{y} \\ & \vdots \\ & \text { ín } \end{aligned}$ | $\begin{aligned} & = \\ & \text { in } \\ & \hline \end{aligned}$ | \＃ | $\begin{aligned} & = \\ & \text { = } \end{aligned}$ | $\begin{gathered} ={ }_{\infty}^{\infty} \\ \hat{N}^{\infty} \end{gathered}$ | $\begin{aligned} & = \\ & m^{\infty} \\ & { }^{\infty} \end{aligned}$ | $\begin{aligned} & = \\ & m^{\sigma} \\ & \hline \end{aligned}$ | $\begin{aligned} & = \\ & =\infty \\ & \infty \end{aligned}$ | $\begin{aligned} & =\infty \\ & N^{\infty} \end{aligned}$ | $\frac{=}{6}$ | $\begin{aligned} & =\infty \\ & i^{\infty} \\ & L^{\circ} \end{aligned}$ | $\stackrel{=}{\sigma}$ | ＊ | ＊ |  |
|  |  | － | \％ | \％ | \％ | \％ | \％ | \％ | \％ | \％ | 幺 | \％ | \％ | \％ | $\begin{aligned} & =\infty \\ & \wedge^{\infty} \\ & o \end{aligned}$ | $\begin{aligned} & = \\ & m^{\gamma} \end{aligned}$ |  |
|  |  | ${ }^{\sim}$ | $\begin{aligned} & = \\ & i \\ & i \\ & i \end{aligned}$ | $\begin{aligned} & e_{\infty} \\ & \hat{N}_{0}^{0} \\ & \vdots \\ & \vdots \end{aligned}$ | $\begin{aligned} & = \\ & m^{\infty} \\ & \vdots \\ & i \end{aligned}$ | $\begin{aligned} & = \\ & n^{\sigma} \\ & \vdots \end{aligned}$ | $\begin{aligned} & = \\ & \underset{\sim}{*} \\ & \vdots \end{aligned}$ | $\begin{aligned} & = \\ & i^{\infty} \\ & \sim \\ & i \\ & i \end{aligned}$ | $\begin{aligned} & \bar{\sim} \\ & \vdots \\ & \vdots \end{aligned}$ | $\begin{aligned} & = \\ & \frac{N}{m} \\ & \stackrel{1}{4} \end{aligned}$ | $\begin{aligned} & \bar{i} \\ & i \end{aligned}$ | $\begin{aligned} & = \\ & m^{\infty} \\ & \vdots \\ & i \\ & i \end{aligned}$ | $\begin{aligned} & = \\ & \wedge_{\infty} \\ & \vdots \\ & \vdots \\ & i \end{aligned}$ | $\begin{aligned} & = \\ & m^{\infty} \\ & \sim \\ & \vdots \\ & \vdots \end{aligned}$ | $\begin{aligned} & = \\ & m^{*} \\ & \sim^{\prime} \\ & \vdots \end{aligned}$ | $\begin{aligned} & = \\ & \vdots \\ & i \\ & i \end{aligned}$ |  |
|  | $I M P H{ }^{\prime} Z I-S U!M{ }^{Z}, I I$ | $\chi^{-}$ | $\begin{aligned} & = \\ & 0 \\ & i \\ & i \end{aligned}$ | $\begin{aligned} & \overline{0} \\ & \vdots \\ & i \end{aligned}$ | $\begin{aligned} & =\infty \\ & { }^{\infty} \\ & = \end{aligned}$ | $\begin{aligned} & = \\ & =\infty \\ & =1 \end{aligned}$ | $\begin{aligned} & =\infty \\ & n^{\infty} \\ & 0 \end{aligned}$ | $\begin{aligned} & = \\ & =0 \\ & 0 \end{aligned}$ | $\begin{aligned} & = \\ & n^{\infty} \\ & n^{\infty} \end{aligned}$ | ō | $\begin{aligned} & = \\ & i \infty \\ & i \end{aligned}$ | ${ }_{N}^{M}$ | ミ | $\begin{aligned} & = \\ & =-\infty \\ & e^{\infty} \end{aligned}$ | in | $\dot{*}$ |  |
|  |  | $\times$ | \％ | \％ | ¢ | \％ | \％ | \％ | \％ | 幺 | \％ | ¢ | $\bar{\circ}$ | ¢ | os | $\overline{=}$ |  |
|  |  | ${ }^{\sim}$ | $\begin{aligned} & \equiv \\ & \vdots \\ & \therefore \end{aligned}$ | $\begin{aligned} & ={ }^{\infty} \\ & n^{\infty} \\ & i \\ & i \end{aligned}$ | $\begin{aligned} & \sum^{\nabla} \\ & \therefore \\ & \therefore \end{aligned}$ | $$ | $\begin{aligned} & = \\ & \sim \\ & i \\ & i \end{aligned}$ | $\begin{aligned} & \overline{\mathrm{i}} \\ & \vdots \\ & \vdots \end{aligned}$ | $\begin{aligned} & ={ }^{\infty} \\ & n^{\infty} \\ & { }^{1} \end{aligned}$ | $\begin{aligned} & = \\ & m^{*} \\ & M \\ & \vdots \\ & i \end{aligned}$ | $\begin{aligned} & =\infty \\ & \stackrel{\infty}{+} \\ & \stackrel{1}{4} \end{aligned}$ | $\begin{aligned} & i^{\infty} \\ & n^{\circ} \\ & \vdots \\ & \vdots \end{aligned}$ | $\begin{aligned} & \text { in } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & = \\ & \text { in } \\ & \text { in } \end{aligned}$ |  | $\begin{aligned} & =\infty \\ & m^{\infty} \\ & 6 \\ & \vdots \end{aligned}$ |  |
|  |  | $x^{-7}$ | ミ <br> I <br> － | $\begin{aligned} & =y_{\infty} \\ & 0^{\infty} \\ & 0 \\ & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & = \\ & 0 \\ & 0 \\ & \vdots \\ & \vdots \end{aligned}$ | $\begin{aligned} & = \\ & n^{*} \end{aligned}$ | $\begin{aligned} & =\infty \\ & { }^{\infty} \\ & \end{aligned}$ | $\begin{aligned} & = \\ & \wedge_{i}^{\infty} \\ & 0 \end{aligned}$ | $\begin{aligned} & = \\ & \text { = } \\ & \hline \end{aligned}$ | ¢ | $\begin{aligned} & = \\ & \text { is } \end{aligned}$ | ¢ | $\begin{aligned} & =\infty \\ & m_{\infty}^{\infty} \\ & \end{aligned}$ | $\begin{aligned} & ={ }^{+\infty} \\ & n^{\infty} \end{aligned}$ | $\begin{aligned} & ={ }^{\infty} \\ & \hat{0}^{\prime} \end{aligned}$ | $\begin{gathered} = \\ M^{\top} \\ n^{*} \end{gathered}$ |  |
|  |  | × | \％ | os | \％ | \％ | \％ | \％ | \％ | \％ | os | \％ | 幺 | 幺 | 亏 | os |  |
|  | 3$\substack{0 \\ 6}$ |  | $\bigcirc$ | $\stackrel{\circ}{\circ}$ | $\stackrel{\circ}{\circ}$ | $\xrightarrow[0]{\circ}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\circ} \\ & \hline \end{aligned}$ | $\stackrel{\circ}{\sim}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\circ} \\ & \hline \end{aligned}$ | $\begin{aligned} & \circ \\ & i n \\ & M \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\rightharpoonup}{\gamma} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{i}{7} \\ & \hline \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\circ} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{i}{n} \\ & \hline \end{aligned}$ | $\begin{aligned} & \circ \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \circ \\ & i \\ & 0 \end{aligned}$ |  |

Figure 4．1．5－4

## DESIGN EXAMPLE

(Typical calculation of headwall corner dimensions)
For condition of $4^{\prime \prime}$ offset.

$$
\begin{aligned}
& x=9^{\prime \prime} \\
& x_{1}=9^{\prime \prime}+\frac{12^{\prime \prime}}{\sin \left(\frac{90^{\circ}-\theta}{2}\right)}-\frac{T+4^{\prime \prime}}{\operatorname{Tan}\left(\frac{90^{\circ}-\theta}{2}\right)} \geqslant 4^{\prime \prime} \\
& x_{2}=9^{\prime \prime}+\frac{12^{\prime \prime}}{\sin \left(\frac{90^{\circ}+\theta}{2}\right)}-\frac{T+4^{\prime \prime}}{\operatorname{Tan}\left(\frac{90^{\circ}+\theta}{2}\right)}
\end{aligned}
$$

For condition where $X_{1}$ is computed to be less than or equal to $4^{\prime \prime}$, use the following equations:

Set $x_{1}=4^{\prime \prime}$, and find $x$ as follows:
$x=4^{\prime \prime}+\frac{T+4^{\prime \prime}}{\operatorname{Tan}\left(\frac{90^{\circ}-\theta}{2}\right)}-\frac{12^{\prime \prime}}{\sin \left(\frac{90^{\circ}-\theta}{2}\right)}$
$x_{2}=9^{\prime \prime}+\frac{12^{\prime \prime}}{\sin \left(\frac{90^{\circ}+\theta}{2}\right)}-\frac{T+4^{\prime \prime}}{\operatorname{Tan}\left(\frac{90^{\circ}+\theta}{2}\right)}$
Given: (Skew Angle) $\theta=30^{\circ}$. (Wingwall Thickness) $T=8^{\prime \prime}$
$x=9^{\prime \prime}$
$x_{1}=9^{\prime \prime}+\frac{12^{\prime \prime}}{\sin \left(\frac{90^{\circ}-30^{\circ}}{2}\right)}-\frac{8^{\prime \prime}+4^{\prime \prime}}{\operatorname{Tan}\left(\frac{90^{\circ}-30^{\circ}}{2}\right)}=12.215^{\prime \prime}$ Use $12^{\prime} 4^{\prime \prime}$
$x_{2}=9^{\prime \prime}+\frac{12^{\prime \prime}}{\sin \left(\frac{90^{\circ}+30^{\circ}}{2}\right)}-\frac{8^{\prime \prime}+4^{\prime \prime}}{\operatorname{Tan}\left(\frac{90^{\circ}+30^{\circ}}{2}\right)}=15.927^{\prime \prime}$ Use $15^{7} 8^{\prime \prime}$


### 4.2 Horizontal Cantilever

Horizontal cantilever wingwalls shall be used if the wingwall is less than or equal to 16 feet in length and the wingwall location can be adequately dewatered.

### 4.2.1 Details

Details for horizontal cantilever wingwalls are given in Figure 4.2.1-1. The design length of the wingwall, L , is calculated using the procedure and figures found in Section 4.1.3.1.

For all culverts with horizontal cantilever wingwalls, a portion of the barrel equal to the minimum of half the wingwall length or six (6) feet shall be poured monolithically with the wingwalls.

If the wingwall thickness exceeds the barrel sidewall thickness by more than two inches, the portion of the barrel wall which must be cast monolithically with the wingwall shall be thickened such that the sidewall thickness is equal to the wingwall thickness. See Figure 4.2.2-1.


Figure 4.2.1-1

### 4.2.2 Design Chart

The thickness of the wingwall and required reinforcement shall be obtained from the horizontal wingwall design chart in Figure 4.2.2-3. Use of this chart requires calculation of a loading constant " $C$," which is based upon the wingwall geometry and the angle of backslope. The procedure for the calculation of " $C$ " is given in Figure 4.2.2-2. Calculation of $P_{A}$ and $P_{B}$ requires calculation of the effective backslope angle using the procedure in Section 4.1.1.2. A detailed example of all of these calculations is given in Section 4.2.3.

The termination of the wall thickness curves at the upper end of the chart reflect the use of a maximum reinforcement ratio of one half of $0.75 \rho_{\mathrm{b}}$.

The area of steel required per foot of wall height will determine the $h_{6}$ or $h_{8}$ bar spacing and size. The values for area of steel on the chart are based on assumed bar sizes, and therefore the reinforcement sizes shall be as specified in the table below. The minimum flexural reinforcement shall be \#4 bars spaced at 12 inch centers. The $h_{3}$ and $h_{7}$ bars shall be the same size as the $h_{6}$ and $h_{8}$ bars, respectively.

| Area of <br> Reinforcement | Bar <br> Size |
| :---: | :---: |
| $0.2-0.47$ | $\# 4$ |
| $0.47-0.74$ | $\# 5$ |
| $0.74-1.06$ | $\# 6$ |
| $1.06-1.44$ | $\# 7$ |
| $>1.44$ | $\# 8$ |

## Table 4.2.2-1



Figure 4.2.2-2


Figure 4.2.2-3

### 4.2.3 Design Examples

## EXAMPLE 1

GIVEN: Backslope Perpendicular to Wall $=1: 3(\mathrm{~V}: \mathrm{H})$
Distance to Break in Slope $=12 \mathrm{ft}$.
Max. Wingwall Height from Invert to Top of Wall $=7 \mathrm{ft}$.
Min. Wingwall Height from Invert to Top of Wall $=3.5 \mathrm{ft}$.
Wall Length $=10 \mathrm{ft}$.


From Table 4.1.1.2-1, For $B=16$ degrees, horizontal pressure $=65 \mathrm{psf}$

$$
\begin{aligned}
\mathrm{P}_{\mathrm{A}} & =(65 \mathrm{psf})(7 \mathrm{ft} .) \quad=\quad 455 \mathrm{lbs} . / \mathrm{ft} . \\
\mathrm{P}_{\mathrm{B}} & =(65 \mathrm{psf})(3.5 \mathrm{ft} .)=227.5 \mathrm{lbs} . / \mathrm{ft} . \\
\mathrm{C} & =\frac{1.35}{6}(455 \mathrm{lbs} . / \mathrm{ft}+2(227.5 \mathrm{lbs} . / \mathrm{ft})) \\
& =205 \mathrm{lbs} . / \mathrm{ft} . \\
\mathrm{M} & =(205 \mathrm{lbs} . / \mathrm{ft})(10 \mathrm{ft} .)^{2}=20500 \mathrm{lb} .-\mathrm{ft} .=20.5 \mathrm{k} \mathrm{ft} .
\end{aligned}
$$

Enter chart at C = 205, extend line horizontally to the intersection of vertical length of wall ( $\mathrm{L}=$ 10 ft .) line, and project a line parallel to moment curve. At the intersection of the thinnest wall thickness curve ( 9 " wing), project a line horizontally to area of reinforcement, and read As = $0.82 \mathrm{in}^{2}$ per foot. Referring to the table above, a \#8 bar should be used, making the size and spacing of $h_{6}$ or $h_{8}$ bars \#8 @ 11" cts.

## EXAMPLE 2

GIVEN: $\quad$ Backslope Perpendicular to Wall $=1: 2(\mathrm{~V}: \mathrm{H})$
Distance to Break in Slope $=30 \mathrm{ft}$.
Max. Wingwall Height from Invert to Top of Wall $=14 \mathrm{ft}$.
Min. Wingwall Height from Invert to Top of Wall $=8 \mathrm{ft}$.
Wall Length $=14 \mathrm{ft}$.


From Table 4.1.1.2-1, For B = 26.56 degrees, horizontal pressure $=71 \mathrm{psf}$

$$
\begin{array}{rlrl}
\mathrm{P}_{\mathrm{A}} & = & (71 \mathrm{psf})(14 \mathrm{ft} .) & = \\
\mathrm{P}_{\mathrm{B}} & = & (71 \mathrm{psf})(8 \mathrm{ft} .) & 994 \mathrm{lbs} . / \mathrm{ft} . \\
\mathrm{C} & = & \frac{1.35}{6}(994 \mathrm{lbs} . / \mathrm{ft}+2(568 \mathrm{lbs} . / \mathrm{ft})) \\
& & & \\
& & 479.25 \mathrm{lbs} . / \mathrm{ft} . \\
\mathrm{M} & = & (479.25 \mathrm{lbs} . / \mathrm{ft} .
\end{array}
$$

Enter chart at $C=479$, extend line horizontally to the intersection of vertical length of wall ( $\mathrm{L}=$ 14 ft .) line, and project a line parallel to moment curve. At the intersection of the thinnest wall thickness curve ( $21^{\prime \prime}$ wing), project a line horizontally to area of reinforcement, and read $\mathrm{A}_{\mathrm{s}}=$ $1.24 \mathrm{in}^{2}$ per foot. Referring to the table above, a \#9 bar should be used, making the size and spacing of $h_{6}$ or $h_{8}$ bars \#9 @ 9" cts.

### 4.3 Two-Way Cantilever L-Type

Two-way cantilever L-type wingwalls are adequate for use for wall lengths between 14 and 30 feet.

### 4.3.1 Details

Details for two-way L-type cantilever wingwalls are given in Figures 4.3.1-1 and 4.3.1-2. These walls are connected to the culvert both along the vertical face of the sidewall and along a horizontal face where the footing of the wingwall connects with the bottom slab of the culvert.

Walls and footings less than 10 inches in thickness contain only one row of reinforcement. Walls and footing ten inches or greater contain a second row of reinforcement in the front face of the wall and/or the bottom of the footing. See Figure 4.3.1-1.

Because the L-type wingwall takes two-way action into account in the design, counterforts must be added to the walls on the obtuse corners to ensure this behavior is present. These counterforts contain the same reinforcement used in the design of the wall. See Figure 4.3.1-2.


Figure 4.3.1-1


Figure 4.3.1-2

### 4.3.2 Design Table

The cross sectional dimensions, and size and spacing of main reinforcement bars required for the L-Type wingwalls are tabulated in Table 4.3.2-1 below. The values for a specific stem height are valid for all backfill angles up to 26.56 degrees (equivalent to a $1: 2(\mathrm{~V}: \mathrm{H})$ backslope). Therefore, only the design height is required to obtain a design.

The stem height (Hs), as shown in Figure 4.3.1-1, is the vertical distance from the top of the stem to the invert, or top of footing. A simpler method to approximate this stem height is obtained by adding the clear height of the barrel to the top slab thickness and the headwall height and then subtracting an amount ( 1 " to $61 / 2^{\prime \prime}$ ) to obtain an even six-inch increment.

Figure 4.3.1-1 shows the nomenclature used in the presentation of the tables. It should be noted that in the case of the v-bars, subscripts "i" and "j" have been used so that those subscripts can assume individual values on the plans for various groups of bars, e.g., v5, v6, v2, etc.

TWO-WAY CANTILEVER L-TYPE WINGWALLS

| STEM |  |  | FOOTING |  | v1(E) BARS |  |  |  |  | z BARS |  | h(E) BARS |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{H}_{5}$ | T | T | B | $\mathrm{T}_{\text {f }}$ | SIZE | SPA. | A | B | C | SIZE | SPA. | SIZE | SPA. |
| ft. - in. | ft. - in. | ft. - in. | ft. - in. | ft. - in. | \# | in. | ft. - in. | ft - in. | ft. - in. | \# | in. | \# | in. |
| 3' - 0" | 0' - 6" | 0'-6" | 1'-8" | 0'-6" | 4 | 12 | 0' - 6" | 5'-11" | 2'-7" | 4 | 12 | 4 | 12 |
| 3' - 6" | $0^{\prime}$ - 6" | 0' - 6" | 1'-8" | 0' - 6" | 4 | 12 | 0' - 6" | 5'-11" | 2' -7" | 4 | 12 | 4 | 12 |
| 4' - 0 " | 0' - 6" | 0' - 6" | 1'-11" | 0' - 6" | 4 | 12 | 0' - 6" | 5'-11" | 2' -7" | 4 | 12 | 4 | 12 |
| $4^{\prime}-6^{\prime \prime}$ | $0^{\prime}-6^{\prime \prime}$ | 0'-6" | 2' - 1' | 0' - 6" | 4 | 10 | 0' - 6' | 5'-11" | 2'-7" | 4 | 12 | 4 | 10 |
| 5' - 0" | 0' - 6" | 0' - 6" | 2' - ${ }^{\prime \prime}$ | 0' - 6" | 4 | 8 | 0' - 6" | 5'-11" | 2'-7" | 4 | 10 | 4 | 8 |
| 5' - 6" | $0^{\prime}$ - 6" | 0' - 6" | 2' - 7' | 0' - 6" | 4 | 7 | 0' - 6" | 5'-11" | 2' -7" | 4 | 7 | 4 | 7 |
| 6' - 0" | 0' - 6" | 0' - 6" | 2'-10" | 0' - 6" | 4 | 6 | 0' - 6" | 5'-11" | 2'-7" | 4 | 6 | 4 | 6 |
| 6' - 6" | 0' - 7" | 0' - 7' | 3'-1" | 0' - 7' | 4 | 5 | 0' - 6" | 5'-11" | 2' -7" | 4 | 5 | 4 | 5 |
| 7' - 0" | 0' - 7' | 0' - 7' | 3' - 4' | 0' - 7' | 4 | 5 | 0' - 6" | 5'-11" | 2' -7" | 4 | 5 | 4 | 5 |
| 7'-6" | 0' -8" | 0' - 8' | 3' - 7" | 0'-8' | 4 | 5 | 0'-6" | 5'-11" | 2'-7" | 4 | 5 | 4 | 5 |
| 8' - 0' | 0' - 8' | 0'-8" | 3'-10" | 0' - 8' | 5 | 6 | 0' - 7' | 6'-5" | 3' -0" | 5 | 6 | 5 | 6 |
| 8' - 6" | 0' - 9" | 0' - 9" | 4'-1" | 0' - 9" | 5 | 6 | 0' - 7' | 6' - 5" | 3' -0" | 5 | 6 | 5 | 6 |
| 9' - 0" | 0' - 9" | 0' - 9' | 4' - 5" | 0' - 9" | 5 | 5 | 0' - 7' | 6' - 5' | 3' -0" | 5 | 5 | 5 | 5 |
| 9'-6" | 0' - 10" | 0'-10' | 4' - 8" | 0'-10' | 5 | 5 | 0'-7" | 6' ${ }^{\prime \prime}$ " | 3' - 0" | 5 | 5 | 5 | 5 |
| 10' - 0" | $0^{\prime}-10{ }^{\prime \prime}$ | 0' - 10" | 4'-11" | $0^{\prime}-10$ | 5 | 5 | 0' - 7' | 6' - 5" | 3' -0" | 5 | 5 | 5 | 5 |
| 10'-6" | 0'-11" | 0'-11' | 5'-2" | 0'-11' | 6 | 6 | 0'-8' | 6'-6" | 3' -0" | 6 | 6 | 6 | 6 |
| 11'-0" | 0'-11" | 0'-11' | 5'-5" | 0'-11" | 6 | 5 | 0'-8' | 6'-6" | 3' -0" | 6 | 5 | 6 | 5 |
| 11'-6" | 1'-0" | 1'-0" | 5' - 8" | 1' - 0" | 6 | 5 | 0' - 8' | 6' - 6"' | 3' - 0" | 6 | 5 | 6 | 5 |
| 12'-0" | 1'-0" | 1'-0" | 5'-11" | 1'-0" | 7 | 6 | 0' - 10" | 6' - 8" | 3' - 0" | 7 | 6 | 7 | 6 |
| 12'-6" | 1'-0" | 1'-0" | 6' - 2" | 1'-0" | 7 | 6 | 0' - 10" | 6' - 8" | 3' - 0" | 7 | 6 | 7 | 6 |
| 13'-0" | 1'-0" | 1'-0" | 6' - 5" | 1'-0" | 8 | 6 | $0^{\prime}-11^{\prime \prime}$ | 6' - 9" | 3' - 0" | 7 | 6 | 8 | 6 |
| 13'-6" | 1'-0" | 1'-2" | 6'-8" | 1'-0" | 8 | 6 | 0'-11" | 6' - 9" | 3' - 0" | 7 | 6 | 8 | 6 |
| 14' - 0' | 1'-0" | 1'-3" | 6'-11" | 1'-0" | 8 | 6 | $0^{\prime}-11^{\prime \prime}$ | 6' -9" | 3' - 0 | 7 | 6 | 8 | 6 |

Table 4.3.2-1

### 4.3.3 Design Example

Given: 6' x 4' Simple Span Box
Top Slab = 6",
Compute Design Stem Height

| Clear Height of barrel | $=$ | $4^{\prime}-0 "$ |
| :--- | :--- | :--- |
| Thickness of top slab | $=$ | $+6^{\prime \prime}$ |
| Headwall | $=$ | $+9^{\prime \prime}$ |
|  | $=$ | $5^{\prime}-3 "$ |
| Subtract (1" to 6 1/2") |  | $-3^{\prime \prime}$ |
| Design Stem Height (Hs) | $=$ | $5^{\prime}-0 "$ |

From the tables for stem height $(\mathrm{Hs})=5^{\prime}-0$ ", find the following:

Stem thickness = T = 6"
Footing width - Stem thickness $=\mathrm{B}-\mathrm{T}=2^{\prime}-5^{\prime \prime}-6 "=1^{\prime \prime}-11^{\prime \prime}$
Footing thickness $=\mathrm{Tf}=6 "$

Stem Reinforcement:

- vi(E) bars: \#4 @ 8"
- h bars: \#4 @ 8"

Footing reinforcement:

- z bars: \#4 @ 10"


### 4.4 Vertical Cantilever T-Type

### 4.4.1 Details

A cross-section for vertical cantilever T-type walls is shown in Figure 4.4.1-1. A front elevation view, including a bar cutting diagram, is shown in Figure 4.4.1-2.

Because of the amount of excavation required for T-type walls adjacent to culverts, barrel cutoff walls for culverts adjacent to T-type walls shall wrap around the sides of the culvert. See Figure 4.4.1-3 for details.


Figure 4.4.1-1


Note: For lengths of minimum lap, see Section 5.

STEM REINFORCEMENT
LAYOUT
Figure 4.4.1-2



Figure 4.4.1-3

### 4.4.2 Table Use

The cross sectional dimensions, and size and spacing of main reinforcement bars required for the T-Type wingwalls are tabulated in the design tables below. To use these tables, the wall height $\left(H_{D}\right)$ and the backslope angle (B) must first be calculated. The wall height $\left(H_{D}\right)$ is the difference between six inches below the top of the wall to the bottom of the footing. See Figure 4.4.1-1. The backslope angle is calculated using the procedure in Figure 4.1.1.2-2.

For most calculations, the resulting value of the backslope angle $B$ will fall between two design rows. When this is the case, the row that requires the wider footing should be used. For small backslope angles, this will be the smaller of the two angles. For large backslope angles, it will be the larger of the two.

Figure 4.4.1-2 shows the nomenclature used in the presentation of the tables. To reduce the amount of lapped steel in the walls, vj bars should be furnished utilizing cutting diagrams.


| VERTICAL CANTILEVER T-TYPE WINGWALLS, DESIGN HEIGHT H ${ }_{0}=\mathbf{7}^{\prime}-6^{\prime \prime}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FILL | BACKSLOPE | STEM |  | FOOTING |  |  | $n(E)$ BARS |  |  |  |  | $v_{i}$ BAR | t, BAR |  | $t_{n}$ BAR |  | $\begin{array}{\|l\|} t_{t}, t_{b} \text { BAR } \\ \hline \text { LENGTH } \\ \hline \end{array}$ | w BAR |  | BEARING PRESSURE |  |
| HEIGHT | ANGLE | T | T | $\mathrm{T}_{\mathrm{f}}$ | b | $X$ | SIZE | SPC. | A | B | C | SIZE | SIZE | SPC. | SIZE | SPC. |  | SIZE | SPC. | SERVICE I | STRENGTHI |
| ft . | degrees | ft. - in. | $\mathrm{ft} .-\mathrm{in}$. | ft. - in. | ft. - in. | ft. - in. | \# | in. | ft. - in. | ft. - in. | ft. - in. | \# | \# | in. | \# | in. | ft . - in. | \# | in. | psf | psf |
| 0 | 0 | 0' - 10" | 0' - 10" | 1'-1" | 4' - 2" | 1'-4" | 4 | 12 | 0' - 6" | 3'-5" | 2'-7" | 4 | 4 | 12 | 4 | 12 | 3'-11" | 4 | 12 | 1650 | 2150 |
| 2.5 | 9 | 0' - 10' | 0' - 10' | 1'-1" | 3'-11" | 1'-4" | 4 | 11 | 0' - 6' | 3'-5" | 2'-7" | 4 | 4 | 12 | 4 | 12 | 3' - 8' | 4 | 12 | 1810 | 2310 |
| 5 | 18 | 0' - 10' | 0' - 10' | 1'-1" | 3'-9' | $1^{\prime}-3^{\prime \prime}$ | 4 | 10 | 0' - 6" | 3'-5" | 2'-7" | 4 | 4 | 12 | 4 | 12 | 3' - 6" | 4 | 12 | 2100 | 2770 |
| $\geq 7.5$ | 26.56 | 0' - 10' | $0^{\prime}-10{ }^{\prime \prime}$ | $1^{\prime}-1{ }^{\prime \prime}$ | 3'-10" | $1^{\prime}-3^{\prime \prime}$ | 4 | 8 | 0' - 6" | 3'-5" | 2'-7" | 4 | 4 | 12 | 4 | 12 | 3'-7" | 4 | 12 | 2500 | 3350 |


| VERTICAL CANTILEVER T-TYPE WINGWALLS, DESIGN HEIGHT H ${ }_{0}=8^{\prime}-0^{\prime \prime}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FILL | BACKSLOPE | STEM |  | FOOTING |  |  | $n(E)$ BARS |  |  |  |  | $\begin{gathered} v_{i} \text { BAR } \\ \text { SIZE } \\ \hline \end{gathered}$ | $t_{+}$BAR |  | $t_{b}$ BAR |  | $t_{t}, t_{b}$ BAR LENGTH | w BAR |  | BEARING PRESSURE |  |
| HEIGHT | ANGLE | T | T | $\mathrm{T}_{\mathrm{f}}$ | b | X | SIZE | SPC. | A | B | C |  | SIZE | SPC. | SIZE | SPC. |  | SIZE | SPC. | SERVICE I | STRENGTH I |
| ft . | degrees | ft. - in. | ft. - in. | ft. - in. | ft. - in. | ft. - in. | \# | in. | ft. - in. | ft. - in. | ft. - in. | \# | \# | in. | \# | in. | ft . - in. | \# | in. | psf | psf |
| 0 | 0 | 0'-10" | 0'-10" | 1'-1" | 4'-6" | 1'-6" | 4 | 11 | 0'-6" | 3'-5" | 2'-7" | 4 | 4 | 12 | 4 | 12 | 4'-3" | 4 | 12 | 1330 | 1860 |
| 2.5 | 9 | $0^{\prime}-10{ }^{\prime \prime}$ | 0' - 10" | 1'-1' | 4'-2" | 1'-4" | 4 | 10 | 0' - 6' | 3'-5" | 2'-7" | 4 | 4 | 12 | 4 | 12 | 3'-11' | 4 | 12 | 1930 | 2550 |
| 5 | 17 | 0' - 10" | 0' - 10" | 1'-1' | 4' - 0" | 1'-4" | 4 | 9 | 0' - 6" | 3'-5" | 2'-7" | 4 | 4 | 12 | 4 | 12 | 3' - 9' | 4 | 12 | 2170 | 2940 |
| 7.5 | 25 | $0^{\prime}$ - 10' | 0' - 10' | 1'-1' | 4' - 1' | 1'-4" | 4 | 7 | 0' - 6" | 3'-5" | 2'-7" | 4 | 4 | 12 | 4 | 12 | $3^{\prime}$ - 10' | 4 | 12 | 2630 | 3630 |
| $\geq 10$ | 26.56 | $0^{\prime}-10{ }^{\prime \prime}$ | $0^{\prime}-10{ }^{\prime \prime}$ | $1^{\prime}-1{ }^{\prime \prime}$ | 4'-1" | 1'-4" | 4 | 7 | $0^{\prime}-6{ }^{\prime \prime}$ | 3'-5" | 2'-7" | 4 | 4 | 12 | 4 | 12 | $3^{\prime}-10{ }^{\prime \prime}$ | 4 | 12 | 2630 | 3630 |


| VERTICAL CANTILEVER T-TYPE WINGWALLS, DESIGN HEIGHT H ${ }_{0}=8^{\prime}-6{ }^{\prime \prime}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FILL | BACKSLOPE | STEM |  | FOOTING |  |  | $\mathrm{n}(\mathrm{E})$ BARS |  |  |  |  | $v_{i}$ BAR | $t_{1}$ BAR |  | $t_{0}$ BAR |  | $t_{1} t_{n} \text { BAR }$ <br> LENGTH | w BAR |  | BEARING PRESSURE |  |
| HEIGHT | ANGLE | T | $\mathrm{T}_{1}$ | $\mathrm{T}_{f}$ | b | $X$ | SIZE | SPC. | A | B | C | SIZE | SIZE | SPC. | SIZE | SPC. |  | SIZE | SPC. | SERVICE I | STRENGTHI |
| ft . | degrees | ft. - in. | ft. - in. | ft. - in. | ft. - in. | ft. - in. | \# | in. | ft. - in. | ft. - in. | ft. - in. | \# | \# | in. | \# | in. | ft . - in. | \# | in. | psf | psf |
| 0 | 0 | 0' - 10" | 0' - 10' | 1'-1" | 4'-9" | 1'-7" | 4 | 9 | 0' - 6" | 3'-5" | 2'-7" | 4 | 4 | 12 | 4 | 12 | 4'-6" | 4 | 12 | 1770 | 2320 |
| 2.5 | 8 | 0' - 10' | 0' - 10' | 1'-1" | 4'-5" | $1^{\prime}-6{ }^{\prime \prime}$ | 4 | 9 | 0' - 6" | 3'-5" | 2'-7" | 4 | 4 | 12 | 4 | 12 | 4' - 2" | 4 | 12 | 1990 | 2710 |
| 5 | 16 | 0' - 10' | 0' - 10' | 1'-1" | 4'-3" | $1^{\prime}-5^{\prime \prime}$ | 4 | 8 | 0' - 6" | 3'-5" | 2'-7" | 4 | 4 | 12 | 4 | 12 | 4' - 0 " | 4 | 12 | 2270 | 3150 |
| 7.5 | 24 | $0^{\prime}-10{ }^{\prime \prime}$ | 0' - 10" | 1'-1" | 4'-3" | $1^{\prime}-5^{\prime \prime}$ | 4 | 7 | 0' - 6" | 3'-5" | 2'-7" | 4 | 4 | 12 | 4 | 12 | 4' - 0 | 4 | 12 | 2680 | 3790 |
| $\geq 10$ | 26.56 | $0^{\prime}$ - 10' | 0' - 10' | 1'-1" | 4'-4" | $1^{\prime}-6^{\prime \prime}$ | 4 | 6 | 0' - 6" | 3'-5" | 2'-7" | 4 | 4 | 12 | 4 | 12 | $4^{\prime}-1$ ' | 4 | 12 | 2750 | 3850 |


| VERTICAL CANTLLEVER T-TYPE WINGWALLS, DESIGN HEIGHT H ${ }_{0}=9^{\prime}-0^{\prime \prime}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FILL HEIGHT | BACKSLOPE <br> ANGLE | STEM |  | FOOTING |  |  | $\mathrm{n}(\mathrm{E})$ BARS |  |  |  |  | vi BAR | t, BAR |  | $t_{0}$ BAR |  | $t, t_{n}$ BAR | w BAR |  | BEARING PRESSURE |  |
|  |  | T | $\mathrm{T}_{1}$ | T, | b | $x$ | SIZE | SPC. | A | B | C | SIZE | SIZE | SPC | SIZE | SPC. | LENGTH | SIZE | SPC. | SERVICEI | StRENGTH |
| ft. | degrees | ft. - in. | At. - in. | ft. - in. | ft. - in. | ft. -in. | \# | in. | ft. - in. | ft. -in. | ft. - in. | \# | \# | in. | \# | in. | ft. - in. | \# | in. | osf | pst |
| 0 | 0 | $0^{\prime}-10^{\prime \prime}$ | $0^{\prime}-10^{\prime \prime}$ | $1^{1}-1{ }^{\prime \prime}$ | 5'-1" | $1^{\prime}$ - $8^{\prime \prime}$ | 4 | 8 | $0^{\prime}$ - $6^{\prime \prime}$ | 3'-5" | 2' - 7" | 4 | 4 | 12 | 4 | 12 | $4^{\prime}$ - 10 " | 4 | 12 | 1810 | 2340 |
| 2.5 | 8 | $0^{\prime}$ - $10^{\prime \prime}$ | $0^{\prime}-10^{\prime \prime}$ | 1'-1" | 4'-9" | 1'-7" | 4 | 8 | $0^{\prime}$ - 6" | 3'-5" | 2'-7" | 4 | 4 | 12 | 4 | 12 | $4^{\prime}$ - $6^{\prime \prime}$ | 4 | 12 | 2020 | 2660 |
| 5 | 16 | $0^{\prime}$ - $10^{\prime \prime}$ | $0^{\prime}$ - $10^{\prime \prime}$ | 1'-1" | $4^{\prime}-7{ }^{\text {7 }}$ | $1^{1}$ - $6^{\prime \prime}$ | 4 | 7 | $0^{\prime}$ - $6^{\prime \prime}$ | $3^{\prime}$ - $5^{\prime \prime}$ | 2'-7" | 4 | 4 | 12 | 4 | 12 | $4^{\prime}-4^{\prime \prime}$ | 4 | 12 | 2290 | 3090 |
| 7.5 | 23 | $0^{\prime}$ - $10^{\prime \prime}$ | $0^{\prime}$ - 10 " | 1'-1" | $4^{\prime}-6^{\prime \prime}$ | 1' - ${ }^{\text {" }}$ | 4 | 6 | $0^{\prime}$ - $6^{\prime \prime}$ | $3^{\prime}$ - 5 " | 2'-7" | 4 | 4 | 11 | 4 | 12 | $4^{\prime}-3^{\prime \prime}$ | 4 | 12 | 2670 | 3750 |
| $\geq 10$ | 26.56 | $0^{\prime}$ - $100^{\prime \prime}$ | $0^{\prime}$ - $10^{\prime \prime}$ | $1^{1}$-1" | $4^{\prime}-8^{\prime \prime}$ | 1'-7" | 4 | 6 | $0^{\prime}$ - $6^{\prime \prime}$ | $3^{\prime}$ - 5" | 2'-7" | 4 | 4 | 10 | 4 | 12 | $4^{\prime}-5^{\prime \prime}$ | 4 | 12 | 2830 | 3860 |







| VERTICAL CANTILEVER T-TYPE WINGWALLS, DESIGN HEIGHT H ${ }_{0}=14^{\prime}-6^{\prime \prime}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FILL | BACKSLOPE | STEM |  | FOOTING |  |  | n (E) BARS |  |  |  |  | $v_{i}$ BAR | t, BAR |  | $t_{0}$ BAR |  | $t_{t} t_{b}$ BAR <br> LENGTH | w BAR |  | BEARING PRESSURE |  |
| HEIGHT | ANGLE | T | $\mathrm{T}_{1}$ | $\mathrm{T}_{\mathrm{f}}$ | b | X | SIZE | SPC. | A | B | C | SIZE | SIZE | SPC. | SIZE | SPC. |  | SIZE | SPC. | SERVICE I | STRENGTHI |
| ft . | degrees | ft. - in. | ft. - in. | ft. - in. | ft . - in. | ft. - in. | \# | in. | ft. - in. | ft. - in. | ft. - in. | \# | \# | in. | \# | in. | ft. - in. | \# | in. | psf | psf |
| 0 | 0 | 1'-0" | 1'-0" | 1'-9" | 8'-2" | 2'-8" | 7 | 8 | 0'-10" | 5'-11" | 4'-5" | 6 | 4 | 9 | 4 | 10 | 7'-11" | 4 | 11 | 2620 | 3600 |
| 2.5 | 5 | $1^{\prime}-0^{\prime \prime}$ | $1^{\prime}-0^{\prime \prime}$ | 1'-9" | 7'-9" | 2'-7" | 7 | 7 | 0' - 10" | 5'-11" | 4'-5" | 6 | 4 | 9 | 4 | 10 | 7'-6" | 4 | 11 | 2840 | 3950 |
| 5 | 10 | 1'-0" | $1^{\prime}-0^{\prime \prime}$ | 1'-9" | 7'-7" | 2' - 6" | 7 | 7 | 0' - 10" | 5' - 11" | 4'-5" | 6 | 4 | 8 | 4 | 10 | 7'-4" | 4 | 11 | 3070 | 4310 |
| 7.5 | 15 | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-9" | 7'-5" | 2'-5" | 7 | 7 | 0' - 10" | 5'-11" | $4^{\prime}-5^{\prime \prime}$ | 6 | 4 | 7 | 4 | 10 | 7' - 2" | 4 | 11 | 3370 | 4830 |
| 10 | 19 | $1^{\prime}-0{ }^{\prime \prime}$ | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-9" | 7'-4" | 2'-5" | 7 | 6 | 0' - 10" | 5'-11" | 4'-5" | 6 | 4 | 6 | 4 | 10 | 7'-1' | 4 | 11 | 3690 | 5360 |
| 12.5 | 23 | 1'-0" | 1'-2" | 1'-9" | 7'-3" | 2'-4" | 7 | 6 | 0' - 10" | 5'-11" | 4'-5" | 6 | 4 | 5 | 4 | 9 | 7' - 0" | 4 | 11 | 4200 | 6120 |
| $\geq 15$ | 26.56 | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-2" | 1'-9" | 7'-4" | 2'-5" | 7 | 6 | 0' - 10" | 5'-11" | $4^{\prime}-5^{\prime \prime}$ | 6 | 5 | 8 | 5 | 11 | 7' - 1' | 4 | 11 | 4370 | 6350 |


| VERTICAL CANTILEVER T-TYPE WINGWALLS, DESIGN HEIGHT $H_{0}=15^{\prime}-0^{\prime \prime}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FILL | BACKSLOPE | STEM |  | FOOTING |  |  | $\mathrm{n}(\mathrm{E})$ BARS |  |  |  |  | $v_{i}$ BAR | $\mathrm{t}_{1}$ BAR |  | $t_{n}$ BAR |  | $t_{t}, t_{n} \mathrm{BAR}$ <br> LENGTH | w BAR |  | BEARING PRESSURE |  |
| HEIGHT | ANGLE | T | T | $\mathrm{T}_{\mathrm{f}}$ | b | $X$ | SIZE | SPC. | A | B | C | SIZE | SIZE | SPC. | SIZE | SPC. |  | SIZE | SPC. | SERVICE I | STRENGTH I |
| ft . | degrees | ft. - in. | ft. - in. | ft. - in. | ft. - in. | ft. - in. | \# | in. | ft. - in. | ft. - in. | ft. - in. | \# | \# | in. | \# | in. | ft. - in. | \# | in. | psf | psf |
| 0 | 0 | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-9" | 8' - 6" | 2' - 10" | 7 | 7 | 0' - 10" | 5'-11" | 4'-5" | 6 | 4 | 9 | 4 | 10 | 8' - 3' | 4 | 11 | 2640 | 3610 |
| 2.5 | 5 | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-9" | 8' - 0" | 2' - 8" | 7 | 7 | 0' - 10" | 5'-11" | 4'-5" | 6 | 4 | 8 | 4 | 10 | 7' - 9' | 4 | 11 | 2950 | 4160 |
| 5 | 9 | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-9" | 7' - 9" | 2'-7" | 7 | 6 | 0' - 10" | 5'-11" | 4'-5" | 6 | 4 | 7 | 4 | 9 | 7' - 6" | 4 | 11 | 3360 | 4730 |
| 7.5 | 14 | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-9" | 7'-9" | 2'-7" | 7 | 6 | 0' - 10" | 5'-11" | 4'-5" | 6 | 4 | 7 | 4 | 9 | 7'-6" | 4 | 11 | 3360 | 4730 |
| 10 | 18 | 1'-0" | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-9" | 7'-7" | 2'-6" | 7 | 6 | 0' - 10" | 5'-11" | 4'-5" | 6 | 4 | 6 | 4 | 9 | 7'-4" | 4 | 11 | 3740 | 5470 |
| 12.5 | 23 | 1'-0" | 1'-1" | 1'-9" | 7' - 8' | 2'-7" | 7 | 5 | 0' - 10" | 7' - 0" | 5' -6" | 6 | 4 | 5 | 4 | 8 | 7' - 5' | 4 | 11 | 4090 | 5850 |
| $\geq 15$ | 26.56 | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-2" | 1'-9" | 8'-1" | 2' - 8" | 7 | 5 | $0^{\prime}$ - 10" | 7'-0" | 5'-6" | 6 | 5 | 6 | 4 | 8 | 7'-10' | 4 | 11 | 4220 | 6310 |


| VERTICAL CANTILEVER T-TYPE WINGWALLS, DESIGN HEIGHT H ${ }_{0}=15^{\prime}-6^{\prime \prime}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FILL | BACKSLOPE | STEM |  | FOOTING |  |  | $\mathrm{n}(\mathrm{E}) \mathrm{BARS}$ |  |  |  |  | $\begin{array}{\|c\|} \hline v_{i} B A R \\ \hline \text { SIZE } \\ \hline \end{array}$ | ${ }_{4}{ }_{\text {t }}$ BAR |  | $t_{0}$ BAR |  | $t_{t}, t_{b} B A R$ <br> LENGTH | w BAR |  | BEARING PRESSURE |  |
| HEIGHT | ANGLE | T | $\mathrm{T}_{1}$ | $\mathrm{T}_{\mathrm{f}}$ | b | X | SIZE | SPC. | A | B | C |  | SIZE | SPC. | SIZE | SPC. |  | SIZE | SPC. | SERVICE I | STRENGTHI |
| ft . | degrees | ft. - in. | ft. - in. | ft. - in. | ft. - in. | ft. - in. | \# | in. | ft. - in. | ft. - in. | ft. - in. | \# | \# | in. | \# | in. | ft . - in. | \# | in. | psf | psf |
| 0 | 0 | 1'-0" | 1'-0" | 1'-9" | 8'-9" | 2'-11" | 7 | 7 | 0'-10" | 5'-11" | 4'-5" | 6 | 4 | 8 | 4 | 9 | 8' - 6" | 4 | 11 | 2760 | 3840 |
| 2.5 | 5 | $1^{\prime}$ - 0 " | 1'-0" | 1'-9" | 8' - ${ }^{\prime \prime}$ | 2' - 9' | 7 | 6 | 0'-10" | 5'-11" | 4'-5" | 6 | 4 | 8 | 4 | 9 | 8' - 0' | 4 | 11 | 3020 | 4340 |
| 5 | 9 | $1^{\prime}$ - 0 ' | 1' - 0" | 1'-9" | 8'-1" | 2'-8" | 7 | 6 | $0^{\prime}-10^{\prime \prime}$ | 5' - 11" | 4'-5" | 6 | 4 | 7 | 4 | 9 | 7'-10" | 4 | 11 | 3240 | 4670 |
| 7.5 | 14 | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-0" | 1'-9" | 8' - 0" | 2' - 8" | 7 | 6 | 0' - 10" | 5' - 11" | 4'-5" | 6 | 4 | 6 | 4 | 9 | 7' - 9' | 4 | 11 | 3450 | 4930 |
| 10 | 18 | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-0" | 1'-9" | 7'-11" | 2' - 8" | 7 | 5 | $0^{\prime}-10^{\prime \prime}$ | 7'-0" | 5' - 6" | 6 | 4 | 5 | 4 | 8 | 7' - 8" | 4 | 11 | 3710 | 5350 |
| 12.5 | 22 | $1^{\prime}$ - 0 ' | 1'-1" | 1'-9" | 7' - 10" | 2' - 8' | 7 | 7 | 0' - 10' | 5'-11" | 4'-5" | 6 | 5 | 7 | 5 | 11 | 7' ${ }^{\prime \prime}{ }^{\prime \prime}$ | 4 | 11 | 3900 | 5920 |
| $\geq 15$ | 26 | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-3" | 1'-9" | 8' - 4" | 2'-9" | 7 | 5 | 0'-10" | 7'-0" | 5'-6" | 6 | 5 | 5 | 5 | 10 | 8' - 1' | 4 | 11 | 4340 | 6490 |


| FILL | BACKSLOPE | STEM |  | FOOTING |  |  | n(E) BARS |  |  |  |  | V, DESICN | t, BAR |  | $t_{0}$ BAR |  | $t_{\text {t }} t_{b}$ BAR | w BAR |  | BEARING PRESSURE |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HEIGHT | ANGLE | T | $\mathrm{T}_{1}$ | $\mathrm{T}_{\mathrm{f}}$ | b | X | SIZE | SPC. | A | B | C | SIZE | SIZE | SPC. | SIZE | SPC. | LENGTH | SIZE | SPC. | SERVICE I | STRENGTHI |
| ft . | degrees | ft. - in. | ft. - in. | ft. - in. | ft. - in. | ft. - in. | \# | in. | ft. - in. | ft. - in. | ft. - in. | \# | \# | in. | \# | in. | ft. - in. | \# | in. | psf | psf |
| 0 | 0 | 1'-0" | 1'-0" | 1'-9" | 9'-1" | 3' - 0" | 7 | 6 | 0'-10" | 5'-11" | 4'-5" | 6 | 5 | 10 | 4 | 9 | 8'-10" | 4 | 11 | 2780 | 3820 |
| 2.5 | 4 | 1'-0" | 1' - 0' | 1'-9" | 8'-7' | 2'-10" | 7 | 6 | 0' - 10" | 5'-11" | 4'-5" | 6 | 5 | 9 | 4 | 9 | 8' - 4' | 4 | 11 | 3050 | 4290 |
| 5 | 9 | 1'-0" | 1'-1" | 1'-9" | 8' - 5' | 2' - 9' | 7 | 6 | 0' - 10" | 5' - 11" | 4'-5" | 6 | 5 | 9 | 4 | 9 | 8' - 2' | 4 | 11 | 3280 | 4610 |
| 7.5 | 13 | 1'-0" | 1'-0" | 1'-9" | 8' - 3' | 2' - 9' | 7 | 5 | 0' - 10" | 7' - 0' | 5'-6" | 6 | 5 | 8 | 4 | 8 | 8' - 0' | 4 | 11 | 3520 | 5090 |
| 10 | 17 | 1'-0" | 1'-1" | 1'-9" | 8'-2" | 2'-9" | 7 | 5 | 0'-10" | 7' - 0" | 5' -6" | 6 | 5 | 8 | 4 | 8 | 7'-11" | 4 | 11 | 3770 | 5420 |
| 12.5 | 21 | 1'-0" | 1'-2" | 1'-9" | 8' - 1' | 2' - 9' | 7 | 5 | 0' - 10" | 7' - 0" | 5'-6" | 6 | 5 | 7 | 4 | 7 | 7'-10" | 4 | 11 | 4170 | 6060 |
| $\geq 15$ | 25 | 1'-0" | 1'-5" | 1'-9" | 8' -6" | 2' - 10" | 7 | 5 | 0' - 10" | 7' - 0" | 5' -6" | 6 | 5 | 5 | 4 | 7 | 8' - 3' | 4 | 11 | 4480 | 6790 |



| VERTICAL CANTILEVER T-TYPE WINGWALLS, DESIGN HEIGHT $H_{0}=17^{\prime}-0^{\prime \prime}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FILL | BACKSLOPE | STEM |  | FOOTING |  |  | $\mathrm{n}(\mathrm{E})$ BARS |  |  |  |  | $v_{i}$ BAR | $\mathrm{t}_{1}$ BAR |  | $t_{b}$ BAR |  | $t_{t} t_{b}$ BAR <br> LENGTH | w BAR |  | BEARING PRESSURE |  |
| HEIGHT | ANGLE | T | $\mathrm{T}_{1}$ | $\mathrm{T}_{\mathrm{f}}$ | b | X | SIZE | SPC. | A | B | C | SIZE | SIZE | SPC. | SIZE | SPC. |  | SIZE | SPC. | SERVICE I | STRENGTHI |
| ft . | degrees | ft. - in. | ft. - in. | ft. - in. | ft. - in. | ft. - in. | \# | in. | ft. - in. | ft. - in. | ft. - in. | \# | \# | in. | \# | in. | ft . - in. | \# | in. | psf | psf |
| 0 | 0 | 1'-0" | 1'-0" | 1'-11" | 9'-7" | 3'-2" | 8 | 6 | 0'-11" | 6'-9" | 5'-1" | 7 | 5 | 10 | 4 | 8 | 9'-4' | 4 | 10 | 2950 | 4170 |
| 2.5 | 4 | 1' - 0' | 1' - 0" | $1^{\prime}-11^{\prime \prime}$ | 9'-1" | 3' - 0' | 8 | 6 | 0'-11' | 6' - 9' | 5'-1" | 7 | 5 | 9 | 4 | 8 | 8' - 10" | 4 | 10 | 3230 | 4620 |
| 5 | 8 | 1' - 0" | 1' - 0" | $1^{\prime}-11^{\prime \prime}$ | 8'-11" | 3'-0" | 8 | 6 | 0'-11" | 6' - 9" | 5'-1" | 7 | 5 | 9 | 4 | 8 | 8' - 8' | 4 | 10 | 3420 | 4970 |
| 7.5 | 12 | 1'-0" | $1^{\prime}-1^{\prime \prime}$ | $1^{\prime}$ - 11" | 8'-10" | 2'-11" | 8 | 6 | 0'-11" | 6' - 9' | 5'-1' | 7 | 5 | 8 | 4 | 8 | 8'-7" | 4 | 10 | 3630 | 5150 |
| 10 | 16 | 1' - 0" | $1^{\prime}-1{ }^{\prime \prime}$ | $1^{\prime}-11^{\prime \prime}$ | 8' - 8" | 2' - 10" | 8 | 6 | 0' - 11" | 6' - 9" | 5'-1" | 7 | 5 | 7 | 4 | 8 | 8' - 5' | 4 | 10 | 3980 | 5770 |
| 12.5 | 20 | 1'-0" | 1'-2" | 1'-11" | 8'-7" | 2' - 10" | 8 | 6 | 0'-11' | 6' - 9' | 5'-1' | 7 | 5 | 6 | 4 | 8 | 8'-4" | 4 | 10 | 4340 | 6380 |
| 15 | 24 | 1' - 0' | 1'-5" | $1^{\prime}$ - 11" | 9' - 0' | 3' - 0' | 8 | 6 | 0'-11" | 6' - 9" | 5'-1' | 7 | 5 | 5 | 4 | 7 | 8' - 9' | 4 | 10 | 4540 | 6810 |
| $\geq 17.5$ | 26.56 | $1^{\prime}$ - 0 " | $1^{\prime}-5^{\prime \prime}$ | 1'-11" | $9^{\prime}-0^{\prime \prime}$ | 3'-0" | 8 | 5 | $0^{\prime}-11^{\prime \prime}$ | 8' - 10" | 7'-2" | 7 | 6 | 6 | 4 | 7 | 8'-9" | 4 | 10 | 4790 | 7420 |


| VERTICAL CANTILEVER T-TYPE WINGWALLS, DESIGN HEIGHT H ${ }_{0}=17^{\prime}-6{ }^{\prime \prime}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FILL | BACKSLOPE | STEM |  | FOOTING |  |  | $\mathrm{n}(\mathrm{E})$ BARS |  |  |  |  | $v_{i}$ BAR | ${ }_{4}$ BAR |  | $t_{0}$ BAR |  | $t_{t} t_{b}$ BAR LENGTH | w BAR |  | BEARING PRESSURE |  |
| HEIGHT | ANGLE | T | T | T ${ }_{f}$ | $b$ | $X$ | SIZE | SPC. | A | B | C | SIZE | SIZE | SPC. | SIZE | SPC. |  | SIZE | SPC. | SERVICE I | STRENGTH I |
| ft . | degrees | ft. - in. | ft. - in. | ft. - in. | ft. - in. | ft. - in. | \# | in. | ft . - in. | ft. - in. | ft. - in. | \# | \# | in. | \# | in. | ft . - in. | \# | in. | psf | psf |
| 0 | 0 | 1'-0" | 1'-0" | 1'-11" | 9'-11" | 3'-3' | 8 | 6 | 0'-11" | 6'-9" | 5'-1" | 7 | 5 | 9 | 4 | 8 | 9'-8" | 4 | 10 | 3010 | 4180 |
| 2.5 | 4 | 1'-0" | $1^{\prime}$ - 0' | 1'-11" | 9'-4" | 3' - 1' | 8 | 6 | 0'-11" | 6' -9" | 5'-1" | 7 | 5 | 9 | 4 | 8 | 9'-1' | 4 | 10 | 3320 | 4810 |
| 5 | 8 | 1'-0" | 1'-1' | 1'-11" | 9'-3" | 3' - 1' | 8 | 6 | 0'-11" | 6' -9" | 5'-1" | 7 | 5 | 8 | 4 | 8 | 9'-0" | 4 | 10 | 3460 | 4900 |
| 7.5 | 12 | 1'-0' | 1'-2" | 1'-11" | 9'-0' | 3' - 0' | 8 | 6 | 0'-11" | 6'-9" | 5'-1" | 7 | 5 | 8 | 4 | 8 | 8' - 9' | 4 | 10 | 3750 | 5500 |
| 10 | 16 | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-2" | 1'-11" | 8'-11" | 2'-11" | 8 | 6 | 0'-11" | 6'-9" | 5' - 1" | 7 | 5 | 7 | 4 | 8 | 8' - 8' | 4 | 10 | 4030 | 5860 |
| 12.5 | 20 | 1'-0" | 1'-3" | 1'-11" | 8'-10" | 2'-11" | 8 | 6 | 0'-11" | 6' -9" | 5'-1" | 7 | 5 | 6 | 4 | 7 | 8' - 7' | 4 | 10 | 4370 | 6370 |
| 15 | 23 | $1^{\prime}-0^{\prime \prime}$ | $1^{\prime}-6{ }^{\prime \prime}$ | 1'-11" | 9'-2" | 3'-1" | 8 | 6 | 0'-11" | 6'-9" | 5'-1" | 7 | 5 | 5 | 4 | 7 | 8'-11" | 4 | 10 | 4520 | 6830 |
| $\geq 17.5$ | 26.56 | 1'-0" | $1^{\prime}-7{ }^{\prime \prime}$ | 1'-11" | 9'-3" | 3'-1' | 8 | 6 | 0'-11" | 6' - 9' | 5'-1" | 7 | 6 | 6 | 4 | 6 | 9'-0' | 4 | 10 | 4890 | 7480 |


| FILLHEIGHT | BACKSLOPE <br> ANGLE | STEM |  | FOOTING |  |  | $\mathrm{n}(\mathrm{E}) \mathrm{BARS}$ |  |  |  |  | $\begin{array}{\|c} v_{i} B A R \\ \hline \text { SIZE } \\ \hline \end{array}$ | $t_{4}$ BAR |  | $t_{b}$ BAR |  | $t_{t} t_{b}$ BAR LENGTH | w BAR |  | BEARING PRESSURE |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | T | $\mathrm{T}_{1}$ | $\mathrm{T}_{\mathrm{f}}$ | b | $X$ | SIZE | SPC. | A | B | C |  | SIZE | SPC. | SIZE | SPC. |  | SIZE | SPC. | SERVICE I | STRENGTH I |
| ft . | degrees | ft. - in. | ft. - in. | ft. - in. | ft. - in. | ft. - in. | \# | in. | ft. - in. | ft. - in. | ft. - in. | \# | \# | in. | \# | in. | ft . - in. | \# | in. | psf | psf |
| 0 | 0 | 1'-0" | 1'-1" | 1'-11" | 10'-2" | 3'-4" | 8 | 6 | 0'-11" | 6'-9" | 5'-1" | 7 | 5 | 8 | 4 | 7 | 9'-11' | 4 | 10 | 3100 | 4370 |
| 2.5 | 4 | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-1" | 1'-11" | 9'-8" | 3'-2" | 8 | 6 | $0^{\prime}$ - 11" | 6' - 9" | 5'-1" | 7 | 5 | 8 | 4 | 8 | 9'-5" | 4 | 10 | 3350 | 4700 |
| 5 | 8 | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-2" | $1^{\prime}-11^{\prime \prime}$ | 9' - 6" | 3'-2" | 8 | 6 | 0'-11" | 6'-9" | 5'-1" | 7 | 5 | 8 | 4 | 7 | 9'-3" | 4 | 10 | 3540 | 5040 |
| 7.5 | 12 | 1'-0" | 1'-2" | 1'-11" | 9'-4' | 3'-1" | 8 | 6 | 0'-11" | 6' - 9' | 5'-1' | 7 | 5 | 7 | 4 | 7 | 9'-1' | 4 | 10 | 3800 | 5460 |
| 10 | 16 | 1'-0" | 1'-3" | 1'-11" | 9'-2' | 3'-1' | 8 | 6 | 0'-11" | 6'-9" | 5'-1' | 7 | 5 | 6 | 4 | 7 | 8'-11' | 4 | 10 | 4050 | 5870 |
| 12.5 | 19 | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-4" | 1' - 11" | 9'-1" | 3' - 0" | 8 | 6 | 0'-11" | 6'-9" | 5'-1" | 7 | 5 | 6 | 4 | 7 | 8' - 10" | 4 | 10 | 4410 | 6410 |
| 15 | 23 | 1'-0" | 1'-5" | 1'-11" | 9'-1' | 3' - 0' | 8 | 6 | 0'-11' | 6' - 9' | 5'-1' | 7 | 5 | 5 | 4 | 6 | 8' - 10' | 4 | 10 | 4860 | 7140 |
| $\geq 17.5$ | 26.56 | $1^{\prime}-0{ }^{\prime \prime}$ | 1'-8' | 1'-11" | 9'-6" | 3'-3" | 8 | 6 | $0^{\prime}$ - 11' | 6' - 9' | 5'-1" | 7 | 7 | 7 | 4 | 6 | 9'-3' | 4 | 10 | 4940 | 7540 |




| FILL HEIGHT | BACKSLOPE ANGLE | STEM |  | FOOTING |  |  | $\mathrm{n}(\mathrm{E})$ BARS |  |  |  |  | $v_{\mathrm{i}} \mathrm{BAR}$ | t, BAR |  | $\mathrm{t}_{\mathrm{n}}$ BAR |  | $t_{t} t_{n}$ BAR LENGTH | w BAR |  | BEARING PRESSURE |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | T | $\mathrm{T}_{1}$ | $\mathrm{T}_{\text {f }}$ | b | X | SIZE | SPC. | A | B | C | SIZE | SIZE | SPC. | SIZE | SPC. |  | SIZE | SPC. | SERVICEI | STRENGTHI |
| ft . | degrees | ft. - in. | ft. - in. | ft. - in. | ft. - in. | ft. - in. | \# | in. | ft. - in. | ft. - in. | ft. - in. | \# | \# | in. | \# | in. | ft. - in. | \# | in. | pst | psf |
| 0 | 0 | 1'-0" | 1'-4" | 2' - 1' | 11'-0" | 3' - 8" | 9 | 7 | 1'-3" | 7' - 6" | 5' -8" | 8 | 6 | 10 | 4 | 7 | 10' - 9' | 4 | 9 | 3310 | 4730 |
| 2.5 | 4 | 1' - 0' | 1'-4" | 2'-1" | 10'-5" | 3' - 6" | 9 | 7 | 1'-3" | 7' - 6" | 5' -8" | 8 | 6 | 10 | 4 | 7 | 10' - 2' | 4 | 9 | 3340 | 4960 |
| 5 | 7 | $1^{\prime}$ - $0^{\prime \prime}$ | 1'-4" | 2' -1" | 10'-3" | 3' - 5" | 9 | 7 | $1^{\prime}-3^{\prime \prime}$ | 7' -6" | 5' -8" | 8 | 6 | 9 | 4 | 7 | 10' - ${ }^{\prime \prime}$ | 4 | 9 | 3540 | 5220 |
| 7.5 | 11 | 1' - $0^{\prime \prime}$ | 1'-4" | 2'-1" | 10'-1" | 3' - 4" | 9 | 7 | $1^{\prime}-3^{\prime \prime}$ | 7' - 6" | 5' - 8" | 8 | 6 | 8 | 4 | 7 | 9' - 10" | 4 | 9 | 3800 | 5680 |
| 10 | 14 | 1' - 0 " | 1' - 4" | 2'-1" | 9'-11" | 3' - 4" | 9 | 6 | 1'-3" | 7' - 6" | 5' - 8" | 8 | 6 | 8 | 4 | 7 | 9' - 8' | 4 | 9 | 4070 | 6160 |
| 12.5 | 18 | 1' - $0^{\prime \prime}$ | 1' - 4" | 2' -1" | 9'-11" | 3' - 4 " | 9 | 6 | 1'-3" | 7' - 6" | 5' - 8" | 8 | 6 | 7 | 4 | 7 | 9' - 8' | 4 | 9 | 4300 | 6350 |
| 15 | 21 | 1' - 0' | 1' - 6" | 2' -1" | 10'-3" | 3' - 5' | 9 | 6 | 1'-3" | 7' -6" | 5' -8" | 8 | 6 | 6 | 4 | 6 | 10' - ${ }^{\prime \prime}$ | 4 | 9 | 4390 | 6760 |
| 17.5 | 24 | 1' - 0' | 1'-9" | 2' - 1 " | 10'-3" | 3' - ${ }^{\prime \prime}$ | 9 | 6 | 1'-3" | 7' -6" | 5' -8" | 8 | 7 | 5 | 4 | 6 | 10' - 0 ' | 4 | 9 | 4990 | 7780 |
| $\geq 20$ | 26.56 | 1' - ${ }^{\prime \prime}$ | 1'-10" | 2'-1" | 10'-4" | 3' - 5" | 9 | 6 | 1'-3" | 7' - 6" | 5' - 8" | 8 | 7 | 5 | 4 | 5 | 10'-1" | 4 | 9 | 5350 | 8100 |

### 4.4.3 Design Example

Given:
Design Height $\left(H_{D}\right)=15^{\prime}-6{ }^{\prime \prime}$
Backslope Angle $(\mathrm{B})=3.8^{\circ}$

The backslope angle falls between the $0^{\circ}$ and $5^{\circ}$ lines in the design table. The required footing width for zero backslope is $8^{\prime}-9^{\prime \prime}$. The required footing width for a $5^{\circ}$ backslope is $8^{\prime}-3^{\prime \prime}$.
Therefore, use the design for a zero backslope condition.

Dimensions:

- Stem thickness at top $=T=12 "$
- Stem thickness at bottom $=\mathrm{T} 1=12^{\prime \prime}$
- Footing thickness $=T f=1^{\prime}-9{ }^{\prime \prime}$
- Footing width $=\mathrm{b}=8^{\prime}-9^{\prime \prime}$
- Toe dimension $=\mathrm{X}=$ 2' $^{\prime}$-11'

Stem Reinforcement:

- n(E) bars \#7 @ 7" cts
- vibars \#6 @ 7" cts

Footing Reinforcement:

- t bars \#4 at 8" cts Heel (top)
- \#4 at 10" cts toe (bottom)
- Length 8'-6"

Maximum Applied Service Bearing Pressure $\mathrm{Q}_{\max }$ : 2460 psf.

Check this maximum applied service bearing pressure with that allowed for the encountered conditions. If the allowable bearing capacity of the soil is less than this pressure, the wingwall should then be considered a special structural design problem, and, therefore, submitted to the Bureau of Bridges and Structures for analysis.

## Section 5 Design Aids

5.1 General

| $\begin{aligned} & \text { Z } \\ & \stackrel{y}{\lambda} \\ & 仓 \\ & 山 己 心 \end{aligned}$ |  | Y | ¢ | ¢ | ㄹ | $\bigcirc$ | － | $\bar{n}$ | $\stackrel{\square}{\square}$ | ${ }_{\circ}^{0} 0$ | $\overbrace{0}^{2}$ | 荿 | \％ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ミ | 1 13 0 | ？ | $\cong$ | へ | ¢ | M | จo | ¢ 0 | $\stackrel{\circ}{\circ} \mathrm{m}$ | $\stackrel{7}{2}$ | $\stackrel{\infty}{\sim}$ | ¢ |
|  |  | $\bigcirc$ | 1 <br> 0 <br> 0 |  | $\cdots$ | ソ | $\stackrel{\square}{\square}$ | n！ | กฺ ${ }_{\text {® }}^{\text {® }}$ | N | $\cdots$ | $\stackrel{\sim}{n}$ | $\xrightarrow[\sim]{n}$ |  |
|  | $\begin{aligned} & \dot{\infty} \subseteq \\ & \therefore E \end{aligned}$ | \％ | ¢ | － | ท | $\stackrel{0}{\bigcirc}$ | $\stackrel{0}{0}$ | Ј | 成枵 | O 0 | $\left[\begin{array}{ll} 0 \\ \hline 0 \\ \hline 10 \\ \hline 1 \end{array}\right.$ | $\xrightarrow{9}$ | $\begin{aligned} & 9 \\ & 0 \\ & \hline- \end{aligned}$ |  |
|  | $\begin{aligned} & 20 \\ & \frac{a}{2} \\ & 50 \end{aligned}$ | $i_{i}^{i}$ | $\begin{aligned} & 0 \\ & 0 \\ & \hline \end{aligned}$ | Y | $\cdots$ | $\stackrel{\infty}{\bigcirc}$ | ¢ | $\cdots$ | ¢̣ | ¢0\％ | \％ | 㐫 | $\stackrel{9}{9}$ | $\stackrel{\sim}{0}$ |
| $\begin{aligned} & 1 \\ & 0 \\ & 0 \end{aligned}$ | $$ | ¢ | $0$ | S | $\wedge$ | กั | ¢ | $\bigcirc$ | ¢ ${ }_{0}^{0}$ | ¢ \％ | $\underset{7}{\infty} \underset{\sim}{\infty}$ |  | $8$ |  |
|  | $\frac{0}{8}$ | N | $\begin{aligned} & \infty \\ & 0 \\ & 0 \end{aligned}$ |  | $\stackrel{\sim}{\sim}$ | べ | そ－ | $\stackrel{9}{7}$ | N | ¢\％${ }^{\circ}$ |  | $\begin{array}{ll} 0 \\ 0 \\ 6 \end{array}$ | $\begin{aligned} & \mathrm{m} \\ & 0 \\ & \underset{i}{2} \end{aligned}$ | \％${ }_{0}^{0}$ |
|  | $\begin{aligned} & \therefore \subseteq \\ & c \\ & c \\ & 0 \end{aligned}$ | ミ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \end{aligned}$ | － | 2 | $\stackrel{\sim}{0}$ | $\stackrel{\sim}{8}$ | －${ }_{\text {？}}$ | 长 | $\begin{gathered} m \\ 0 \\ i \end{gathered}$ | $\underset{\sim}{\sim}$ | N | $\stackrel{\imath}{i}$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & \end{aligned}$ |
|  |  | $\frac{=}{6}$ | $\begin{aligned} & 0 \\ & \hline 0 \\ & \hline 1 \end{aligned}$ | $0$ | へ | ¢ | $\stackrel{\circ}{\text { ¢ }}$ | ？ | － 0 | $\mathfrak{z}$ | $\stackrel{\rightharpoonup}{6} \underset{\sim}{n}$ | $\underset{\sim}{\infty}$ | $\stackrel{n}{\sim}$ | io |
|  | ¢W | $\bigcirc$ | $0$ |  | $\underset{\sim}{N}$ | \％ | ภ | ¢ | $\cdots$ | $\underset{\substack{8 \\ \\ \hline \\ 0}}{0}$ | $\stackrel{0}{0}$ | $\begin{array}{\|c\|c} \hline \approx & 8 \\ & 0 \\ \hline \end{array}$ |  | $\stackrel{n}{m}$ |
| 这㞫岕 |  | in | へ | 2 | $\stackrel{\square}{\square}$ | $\stackrel{\text { ¢ }}{\substack{\text { m }}}$ | － | ， | O¢ | $\bar{M}$ | $\underset{6}{\mathrm{O}}$ | $\overbrace{0}^{\infty} \underset{\sim}{\infty}$ | $\begin{aligned} & 0 \\ & \stackrel{0}{2} \\ & \stackrel{n}{2} \\ & \hline \end{aligned}$ |  |
|  |  | in | $\stackrel{\infty}{\square}$ | 0 | へ | ¢ |  | N |  | $\underset{-i}{\underset{i}{2}}$ |  | $\begin{gathered} 0 \\ \hline \end{gathered}$ |  |  |
| $\underset{\substack{0 \\ N}}{\substack{2}}$ |  | $\pi$ | ㄲ | $\stackrel{\text { ci }}{\square}$ | $\stackrel{9}{9}$ | ก | $\stackrel{9}{7}$ | － | $\underset{\sim}{\infty} \underset{\sim}{\infty}$ | $\begin{aligned} & 0 \\ & 6 \\ & -1 \end{aligned}$ |  |  | $\begin{aligned} & \infty \\ & \underset{\sim}{0} \\ & m \\ & =0 \end{aligned}$ |  |
|  |  | － |  |  | M | $\bigcirc$ | ก | Ọ¢ | $\stackrel{\otimes}{\circ} \underset{i}{\sim}$ | $0$ |  |  | $\left[\begin{array}{cc} 8 \\ 0 \\ 0 & 0 \\ 0 & 0 \\ m \end{array}\right.$ |  |
|  |  |  |  | $\stackrel{\square}{6}$ | $\stackrel{60}{n}$ |  | $\begin{aligned} & \infty \\ & \hline 6 \end{aligned}$ | $\stackrel{m}{\substack{0}}$ | $\begin{aligned} & \stackrel{N}{0} \\ & \stackrel{n}{2} \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\square} \\ & \stackrel{y}{*} \end{aligned}$ | $\begin{aligned} & \mathrm{Q} \\ & \stackrel{\rightharpoonup}{\mathrm{o}} \\ & \stackrel{y}{2} \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{4} \\ & \stackrel{1}{4} \end{aligned}$ | $\begin{aligned} & \underset{\sim}{m} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & m \\ & m \\ & m \\ & \text { in } \end{aligned}$ |
|  | $\dot{0}$ |  |  | $\begin{aligned} & 8 \\ & \hline 6 \end{aligned}$ | $\stackrel{\square}{\square}$ |  | $$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{0} \\ & \end{aligned}$ | $\frac{\infty}{7}$ | $\begin{aligned} & \text { en } \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { + } \\ & \end{aligned}$ | $\stackrel{\otimes}{\mathrm{O}}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \end{aligned}$ | 咢 |
|  | $\begin{aligned} & \stackrel{0}{N} \\ & \stackrel{1}{2} \end{aligned}$ |  |  | $\sim$ | $m$ |  | $\checkmark$ | $\checkmark$ | 6 | $\wedge$ | $\infty$ | $\sigma$ | $\bigcirc$ | $\approx$ |

Figure 5．1－1


Figure 5.1-2

## Reinforcement Bar Splices

(for Coated and Uncoated Bars)

## Tension Splices

I. Regions of high tensile stress or

Reinforcement provided < twice that required for strength.

Use Class B splice
II. Regions of low tensile stress or

Reinforcement provided $>$ twice that required for strength.

1. No more than $3 / 4$ of the bars are lap spliced within a required lap length.

Use Class A splice
2. More than $3 / 4$ of the bars are lap spliced within a required lap length.

Use Class B splice
III. Assume all temperature and shrinkage reinforcement fully stressed. A Class B splice must be used depending on amount spliced within required splice length.

Tension Splices for Epoxy Coated Reinforcement in Normal Weight Concrete
(f'c = 3,500psi; fy = 60,000psi)

| Basic Lap |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Bar Size | Min. Cover | Class A (1.0 $\mathrm{I}_{\mathrm{d}}$ ) |  | Class B (1.3 $\mathrm{I}_{\mathrm{d}}$ ) |  |
|  |  | $\begin{gathered} \mathrm{s}<6^{\prime \prime} \\ \mathrm{cts} . \end{gathered}$ | $\begin{gathered} s \geq 6^{\prime \prime} \\ \text { cts. } \end{gathered}$ | $\begin{gathered} \mathrm{s}<6^{\prime \prime} \\ \mathrm{cts} . \end{gathered}$ | $\begin{gathered} s \geq 6^{\prime \prime} \\ \text { cts. } \end{gathered}$ |
| \#4 | $1 "$ | 2'-0" | 2'-0" | 2'-7' | 2'-7" |
| \#5 | 1.5" | 2'-7" | 2'-5" | 3'-4" | 3'-2" |
|  | $1{ }^{\prime \prime}$ | 2'-11" | 2'-11" | 3'-9" | 3'-9" |
| \#6 | 1.5" | 3'-8" | 2'-11" | 4'-9" | 3'-10" |
|  | $1 "$ | 4'-0" | 4'-0" | 5'-2" | 5'-2" |
| \#7 | 2" | 4'-3" | 3'-5" | 5'-6" | 4'-5" |
|  | 1.5 " | 4'-3" | 3'-10" | 5'-6" | 5'-0" |
|  | $1{ }^{\prime \prime}$ | 5'-2" | 5'-2" | 6'-8" | 6'-8" |
| \#8 | 2" | 5'-6" | 3'-11" | 7'-2' | 5'-1" |
|  | 1.5 " | 5'-6" | 4'-10" | 7'-2" | 6'-4" |
|  | $1{ }^{\prime \prime}$ | 6'-5" | 6'-5" | 8'-5" | 8'-5" |
| \#9 | 2.5 " | 7'-0" | 4'-5" | 9'-2" | 5'-8" |
|  | 2" | 7'-0" | 4'-10" | 9'-2" | 6'-3" |
|  | 1.5" | 7'-0" | 6'-0" | 9'-2" | 7'-9" |
|  | $1{ }^{\prime \prime}$ | 7'-10" | 7'-10" | 10'-3" | 10'-3" |
| \#10 | 2.5 " | 7'-10" | 5'-3" | 10'-2" | 6'-9" |
|  | 2" | 7'-10" | 5'-11" | 10'-2" | 7'-8" |
|  | 1.5" | 7'-10" | 7'-4" | 10'-2" | 9'-6" |
|  | $1{ }^{\prime \prime}$ | 9'-6" | 9'-6" | 12'-5" | 12'-5" |
| \#11 | 2.5" | 9'-7" | 6'-5" | 12'-6" | 8'-4" |
|  | 2" | 9'-7" | 7'-1' | 12'-6" | 9'-3" |
|  | 1.5 " | 9'-7" | 8'-9" | 12'-6" | 11'-4" |
|  | $1{ }^{\prime \prime}$ | 11'-3" | 11'-3" | 14'-8" | 14'-8" |


| Horizontal Lap w/>12" Concrete Cast Below |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Bar } \\ & \text { Size } \end{aligned}$ | Min. Cover | Class A (1.0 $\mathrm{I}_{\mathrm{d}}$ ) |  | Class B (1.3 ld) |  |
|  |  | $\begin{gathered} \hline \mathrm{s}<6 " \\ \text { cts. } \\ \hline \end{gathered}$ | $\begin{gathered} s \geq 6^{\prime \prime} \\ \text { cts. } \end{gathered}$ | $\begin{gathered} \mathrm{s}<6^{\prime \prime} \\ \mathrm{cts} . \end{gathered}$ | $\begin{gathered} s \geq 6^{\prime \prime} \\ \text { cts. } \end{gathered}$ |
| \#4 | $1 "$ | 2'-3" | 2'-3" | 2'-11" | 2'-11" |
| \#5 | 1.5" | 2'-11" | 2'-9" | 3'-9" | 3'-7' |
|  | $1{ }^{\prime \prime}$ | 3'-3" | 3'-3" | 4'-3" | 4'-3" |
| \#6 | 1.5" | 4'-2" | 3'-4" | 5'-4" | 4'-4" |
|  | $1{ }^{\prime \prime}$ | 4'-6" | 4'-6" | 5'-10" | 5'-10" |
| \#7 | 2" | 4'-10" | 3'-10" | 6'-3" | 5'-0" |
|  | 1.5" | 4'-10" | 4'-4" | 6'-3' | 5'-8" |
|  | $1{ }^{\prime \prime}$ | 5'-10" | 5'-10" | 7'-7' | 7'-7' |
| \#8 | 2" | 6'-3" | 4'-5" | 8'-2" | 5'-9" |
|  | 1.5" | 6'-3" | 5'-6" | 8'-2" | 7'-2" |
|  | $1 "$ | 7'-4" | 7'-4" | 9'-6" | 9'-6" |
| \#9 | 2.5 " | 8'-0" | 5'-0" | 10'-4" | 6'-5" |
|  | 2" | 8'-0" | 5'-5" | 10'-4" | 7'-1" |
|  | 1.5" | 8'-0" | 6'-9" | 10'-4" | 8'-9" |
|  | $1{ }^{\prime \prime}$ | 8'-11" | 8'-11" | 11'-7" | 11'-7" |
| \#10 | 2.5" | 8'-10" | 5'-11" | 11'-6" | 7'-8' |
|  | $2{ }^{\prime \prime}$ | 8'-10" | 6'-9" | 11'-6" | 8'-9" |
|  | 1.5" | 8'-10" | 8'-3" | 11'-6" | 10'-9" |
|  | $1{ }^{\prime \prime}$ | 10'-10" | 10'-10" | 14'-0" | 14'-0" |
| \#11 | 2.5" | 10'-11' | 7'-3" | 14'-2" | 9'-5" |
|  | 2" | 10'-11" | 8'-1" | 14'-2" | 10'-6" |
|  | 1.5 " | 10'-11" | 9'-10" | 14'-2" | 12'-10" |
|  | $1{ }^{\prime \prime}$ | 12'-9" | 12'-9" | 16'-7" | 16'-7" |

## Notes:

- Confinement reinforcement was conservatively assumed to be zero.
- Larger covers for the smaller bars were intentionally omitted because additional cover does not reduce the lap length.

Tension Splices for Unprotected Reinforcement in Normal Weight Concrete
( f ' $\mathbf{c}=\mathbf{3 , 5 0 0} \mathrm{psi} ; \mathrm{fy}=\mathbf{6 0 , 0 0 0} \mathrm{psi}$ )

| Basic Lap |  |  |  |  |  | Horizontal Lap w/>12" Concrete Cast Below |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bar Size | Min. Cover | Class A (1.0 $\mathrm{I}_{\mathrm{d}}$ ) |  | Class B (1.3 $\mathrm{I}_{\mathrm{d}}$ ) |  | Bar <br> Size | Min. Cover | Class A (1.0 $\mathrm{I}_{\mathrm{d}}$ ) |  | Class B (1.3 Id ${ }_{\text {) }}$ |  |
|  |  | $\begin{gathered} \hline \mathrm{s}<6^{\prime \prime} \\ \mathrm{cts} . \end{gathered}$ | $\begin{gathered} \mathrm{s} \geq 6^{\prime \prime} \\ \text { cts. } \end{gathered}$ | $\begin{gathered} \hline \mathrm{s}<6 " \\ \text { cts. } \end{gathered}$ | $\begin{gathered} s \geq 6^{\prime \prime} \\ \text { cts. } \end{gathered}$ |  |  | $\begin{gathered} \hline \mathrm{s}<6^{\prime \prime} \\ \mathrm{cts} . \end{gathered}$ | $\begin{gathered} \mathrm{s} \geq 6^{\prime \prime} \\ \text { cts. } \end{gathered}$ | $\begin{gathered} \hline \mathrm{s}<6^{\prime \prime} \\ \mathrm{cts} . \end{gathered}$ | $\begin{gathered} s \geq 6^{\prime \prime} \\ \text { cts. } \end{gathered}$ |
| \#4 | $1{ }^{\prime \prime}$ | 1'-4" | 1'-4" | 1'-9" | 1'-9" | \#4 | $1{ }^{\prime \prime}$ | 1'-9" | 1'-9" | 2'-3" | 2'-3" |
| \#5 | 1.5" | 1'-9" | 1'-8" | 2'-3" | 2'-2" | \#5 | 1.5" | 2'-3" | 2'-2" | 2'-10" | 2'-9" |
|  | $1{ }^{\prime \prime}$ | 1'-11" | 1'-11" | 2'-6" | 2'-6" |  | $1{ }^{\prime \prime}$ | 2'-6" | 2'-6" | 3'-3" | 3'-3" |
| \#6 | 1.5 " | 2'-5" | 2'-0" | 3'-2' | 2'-7" | \#6 | 1.5" | 3'-2' | 2'-7' | 4'-1" | 3'-4" |
|  | $1{ }^{\prime \prime}$ | 2'-8" | 2'-8" | 3'-5" | 3'-5" |  | $1{ }^{\prime \prime}$ | 3'-5" | 3'-5" | 4'-6" | 4'-6" |
| \#7 | 2" | 2'-10" | 2'-3' | 3'-8" | 3'-0" | \#7 | 2" | 3'-8" | 3'-0" | 4'-9" | 3'-10" |
|  | 1.5 " | 2'-10" | 2'-7" | 3'-8" | 3'-4" |  | 1.5" | 3'-8" | 3'-4" | 4'-9" | 4'-4" |
|  | $1{ }^{\prime \prime}$ | 3'-5" | 3'-5" | 4'-6" | 4'-6" |  | $1{ }^{\prime \prime}$ | 4'-6" | 4'-6" | 5'-10" | 5'-10" |
| \#8 | 2" | 3'-8" | 2'-7" | 4'-10" | 3'-5" | \#8 | 2" | 4'-10" | 3'-5" | 6'-3" | 4'-5" |
|  | 1.5" | 3'-8" | 3'-3" | 4'-10" | 4'-3" |  | 1.5" | 4'-10" | 4'-3" | 6'-3" | 5'-6" |
|  | $1{ }^{\prime \prime}$ | 4'-4" | 4'-4" | 5'-7" | 5'-7" |  | $1{ }^{\prime \prime}$ | 5'-7" | 5'-7" | 7'-3" | 7'-3" |
| \#9 | 2.5" | 4'-8" | 2'-11' | 6'-1' | 3'-10" | \#9 | 2.5" | 6'-1" | 3'-10" | 7'-11" | 4'-11" |
|  | 2" | 4'-8" | 3'-3" | 6'-1" | 4'-2" |  | 2" | 6'-1' | 4'-2" | 7'-11" | 5'-5" |
|  | 1.5" | 4'-8" | 4'-0" | 6'-1" | 5'-2' |  | 1.5" | 6'-1" | 5'-2' | 7'-11" | 6'-9" |
|  | $1{ }^{\prime \prime}$ | 5'-3' | 5'-3" | 6'-10" | 6'-10" |  | 1" | 6'-10" | 6'-10" | 8'-10" | 8'-10" |
| \#10 | 2.5" | 5'-3" | 3'-6" | 6'-9" | 4'-6" | \#10 | 2.5" | 6'-9" | 4'-6" | 8'-9" | 5'-10" |
|  | 2" | 5'-3' | 4'-0" | 6'-9" | 5'-2" |  | 2" | 6'-9" | 5'-2" | 8'-9" | 6'-8" |
|  | 1.5" | 5'-3' | 4'-11' | 6'-9" | 6'-4" |  | 1.5" | 6'-9" | 6'-4" | 8'-9" | 8'-3' |
|  | $1{ }^{\prime \prime}$ | 6'-4" | 6'-4" | 8'-3" | 8'-3' |  | $1{ }^{\prime \prime}$ | 8'-3" | 8'-3" | 10'-9" | 10'-9" |
| \#11 | 2.5 " | 6'-5" | 4'-4" | 8'-4" | 5'-7" | \#11 | 2.5" | 8'-4" | 5'-7" | 10'-10" | 7'-3' |
|  | 2" | 6'-5" | 4'-9" | 8'-4" | 6'-2" |  | 2" | 8'-4" | 6'-2" | 10'-10" | 8'-0" |
|  | 1.5" | 6'-5" | 5'-10" | 8'-4" | 7'-7" |  | 1.5" | 8'-4" | 7'-7' | 10'-10" | 9'-10" |
|  | 1 " | 7'-6" | 7'-6" | 9'-9" | 9'-9" |  | $1{ }^{\prime \prime}$ | 9'-9" | 9'-9" | 12'-8" | 12'-8" |

Notes:

- Confinement reinforcement was conservatively assumed to be zero.
- Larger covers for the smaller bars were intentionally omitted because additional cover does not reduce the lap length.


Figure 5.1-3


CULVERT EXTENSION WITH
EXISTING HEADWALL REMOVED
Figure 5.1-4


Figure 5.1-5


Note: (to be placed on the plans) Expansion bolts shall be $3_{4}$ " $\phi$ hooked bolts. Hooked bolts shall extend a minimum of 9 " into new concrete.

| Clear Span or Clear Height | No. of ${ }^{3} 4^{\prime \prime} \phi$ Exp. Bolts Req'd per side |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Extension $\leq 15$ |  | Extension > 15' |  |
|  | No. * | Spacing | No. ${ }^{*}$ | Spacing |
| 2.0 | ** | ** | ** | ** |
| 2.5 | 2 | $18^{\prime \prime}$ | 2 | 18" |
| 3.0 | 2 | $24^{\prime \prime}$ | 2 | $24^{\prime \prime}$ |
| 4.0 | 3 | 18" | 3 | 18" |
| 5.0 | 4 | $16^{\prime \prime}$ | 3 | $24^{\prime \prime}$ |
| 6.0 | 5 | $15^{\prime \prime}$ | 4 | 20" |
| 7.0 | 5 | $18^{\prime \prime}$ | 4 | 24" |
| 8.0 | 6 | $17^{\prime \prime}$ | 5 | $21^{\prime \prime}$ |
| 9.0 | 6 | $19^{\prime \prime}$ | 5 | 24" |
| 10.0 | 7 | $18^{\prime \prime}$ | 6 | $21^{\prime \prime}$ |
| 11.0 | 8 | $17^{\prime \prime}$ | 6 | 24" |
| 12.0 | 8 | 19" | 7 | 22" |

Example:
6'x4' box culvert to be extended $18^{\prime}$ at one end only. From table find

6 ' side requires $4-3_{4}^{\prime \prime} \phi$ Expansion bolts at $20^{\prime \prime}$ cts. $4^{\prime}$ side requires $3-3_{4}^{\prime \prime} \phi$ Expansion bolts at $18^{\prime \prime} \mathrm{cts}$.

Total Number required
$(4+3) 2=14-3_{4}^{\prime \prime} \phi$ Expansion Bolts.

* Note: Expansion bolts based on non-skewed culverts.
**Note: Use minimum of one (1) Expansion bolt at each corner.

EXPANSION BOLTS
REQUIRED FOR CULVERT EXTENSIONS

Figure 5.1-6

### 5.2 Base Sheets

Base sheets for culverts and end sections can be found at http://www.idotillinois.gov/doing-business/procurements/engineering-architectural-professional-services/Consultants-

Resources/bridges-and-structures-cadd-downloads-and-guidelines.

